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FIELD BOOK

740

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B. K. ERBOTH COMPANY

PLEASE RETURN TO  
 GAUGA COUNTY ENGINEER

TABLE FOR REDUCING PERCHES TO FEET AND INCHES.

PERCH	FEET.	PERCH.	FEET.	PERCH.	FEET.	PERCH.	FEET.	PERCH.	FEET.	PERCH.	FEET.
1	16.6 in.	21	3.46 6 in.	41	6.76.6 in.	61	10.06.6 in.	81	13.26.6 in.	101	16.50.0
2	33.0	22	3.63.0	42	6.93.0	62	10.23.0	82	13.53.0	102	16.83.0
3	49.6	23	3.79.6	43	7.09.6	63	10.39.6	83	13.89.6	103	17.16.6
4	66.0	24	3.96.0	44	7.26.0	64	10.56.0	84	14.26.0	104	17.50.0
5	82.6	25	4.12.6	45	7.42.6	65	10.72.6	85	14.62.6	105	17.83.6
6	99.0	26	4.29.0	46	7.59.0	66	10.89.0	86	15.09.0	106	18.17.0
7	1.15.6	27	4.45.6	47	7.75.6	67	11.05.6	87	15.55.6	107	18.50.6
8	1.32.0	28	4.62.0	48	7.92.0	68	11.22.0	88	16.02.0	108	18.84.0
9	1.48.6	29	4.78.6	49	8.08.6	69	11.38.6	89	16.48.6	109	19.17.6
10	1.65.0	30	4.95.0	50	8.25.0	70	11.55.0	90	16.95.0	110	19.51.0
11	1.81.6	31	5.11.6	51	8.41.6	71	11.71.6	91	17.41.6	111	19.84.6
12	1.98.0	32	5.28.0	52	8.58.0	72	11.88.0	92	17.88.0	112	20.18.0
13	2.14.6	33	5.44.6	53	8.74.6	73	12.04.6	93	18.34.6	113	20.51.6
14	2.31.0	34	5.61.0	54	8.91.0	74	12.21.0	94	18.81.0	114	20.85.0
15	2.47.6	35	5.77.6	55	9.07.6	75	12.37.6	95	19.27.6	115	21.18.6
16	2.64.0	36	5.94.0	56	9.24.0	76	12.54.0	96	19.74.0	116	21.52.0
17	2.80.6	37	6.10.6	57	9.40.6	77	12.70.6	97	20.20.6	117	21.85.6
18	2.97.0	38	6.27.0	58	9.57.0	78	12.87.0	98	20.67.0	118	22.19.0
19	3.13.6	39	6.43.6	59	9.73.6	79	13.03.6	99	21.13.6	119	22.52.6
20	3.30.0	40	6.60.0	60	9.90.0	80	13.20.0	100	21.60.0	120	22.86.0

COURT HOUSE  
 CHARDON O.  
 PHONE 250-X

B. K. ELLIOTT COMPANY, PITTSBURG, PA.  
 DRAWING MATERIALS AND SURVEYING INSTRUMENTS

(8-61) X-sec #87 to Dines pg. 38  
 Caves Road Russe (1 Twp  
 Section A #157  
 (COVER)

Park Sec B #144

X Sec Chag. Rivir ± 500' EAW pg 50

Cedar Rd Sec A+B  
 Topo pg. 55

Cedar Rd. X section cont.  
 From F.B. 139 pg. 66-74

1961 Caves - Topo Dines to Fairmount  
 Topo 87 to Dines pg. 25-29  
 52-54

137

T.H. #157

CAVE ROAD, Russell Twp.

Page

1 - 23

PEKIN T.H. 144  
Dines Corners Road

Russell (Sec. A)

24 -

20+1928 POT

19+48.3 12" Cor. Iron Pipe

15+61 12" Vit. Pipe.

15+00

11+00 spike, P.O.T.

9+39.66 POT

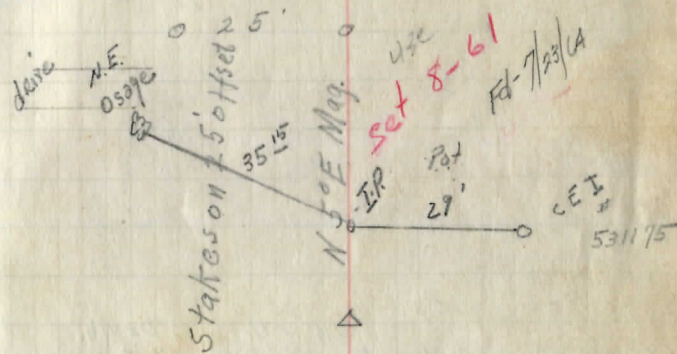
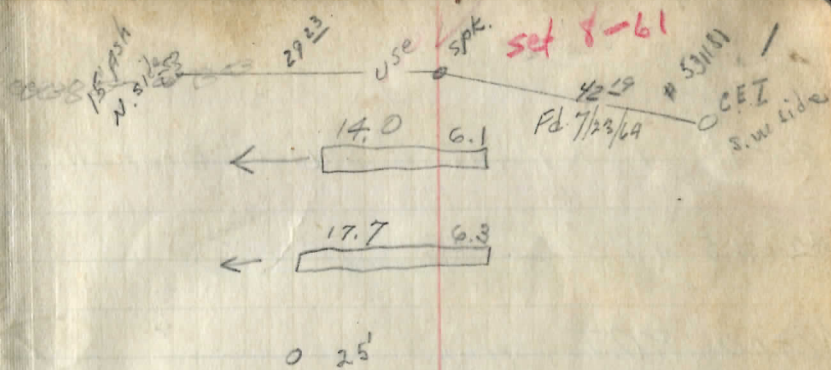
7+86.45 P.O.T. Hub.

5+78

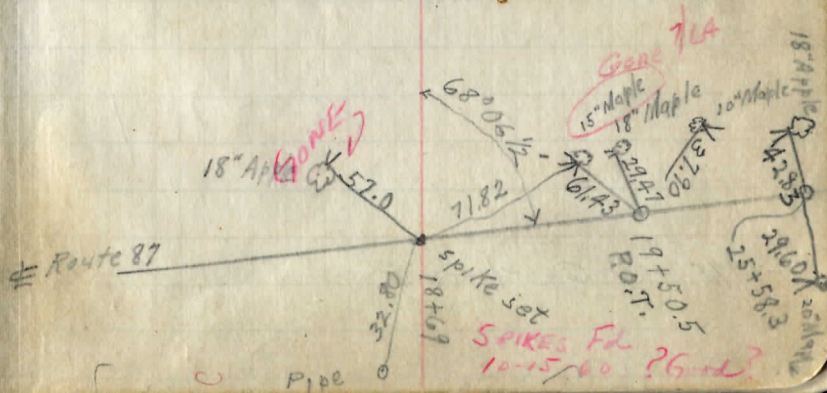
May 4, 1935, Cloudy, 50°  
W.C. Marks, Chas. Rand, F. Bohland

411  
0+00,  $\frac{1}{2}$  of Care Rd.  
Located at Sta. 18+69,  $\frac{1}{2}$  State Route #87

See 1977 for  
1964 Refs



10" vitrified  
Pipe Culvert  $\frac{10' \quad 10''}{\text{stone sluice Vit Pipe}}$



46+91 1' x 1' stone sluice, Broken.

42+96.5

40+00 P.O.T., spike

38+96.5 <sup>probably cast iron</sup> sluice, small, plugged,

34+97.2

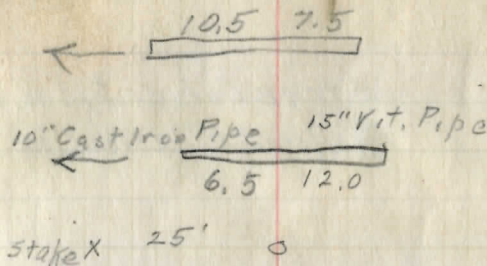
pot

32+14.3 stone Culvert, <sup>Width</sup> 2.5' ± x <sup>Depth</sup> 2 1/2' ±  
Concrete Cover, Forms Left in place  
Side Walls, good

26+00 P.O.T. spike

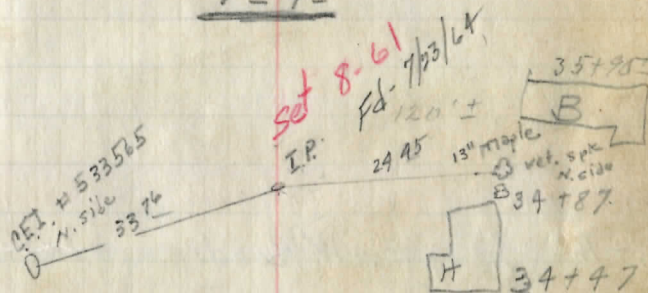
24+99.5 12" Cast Iron Pipe

21+00 P.O.T. spike

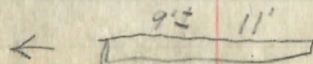
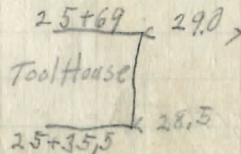
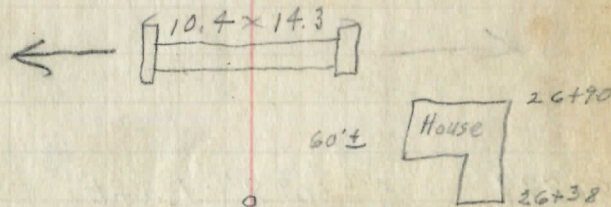


stake x 25' 0

7' ± 9' ±



From Sta. 18 Forward.  
30" Wedge stakes at 25' Offset at Stations that are multiples of 5  
16" Lath " " 15' " other Stations.



1/4th Δ 15' x spike

65+92.5

Stone Culvert, 3' W. X 2' D,  
Walls good, 1 cover stone broken

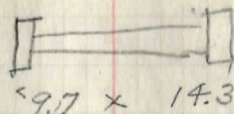
63+16± E of E. + W. Road.

58+79.1 Δ = 0° 8' Left

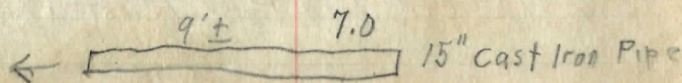
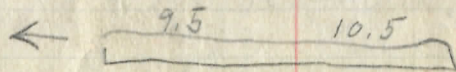
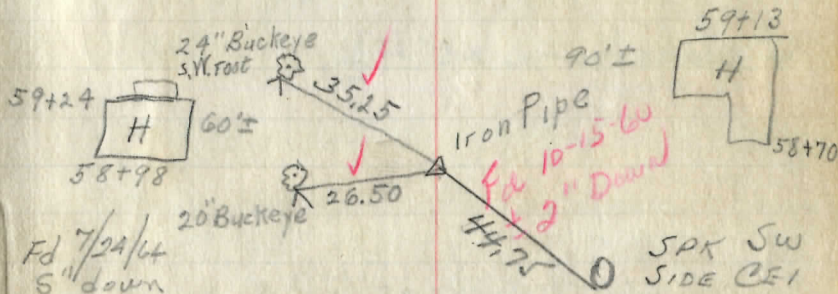
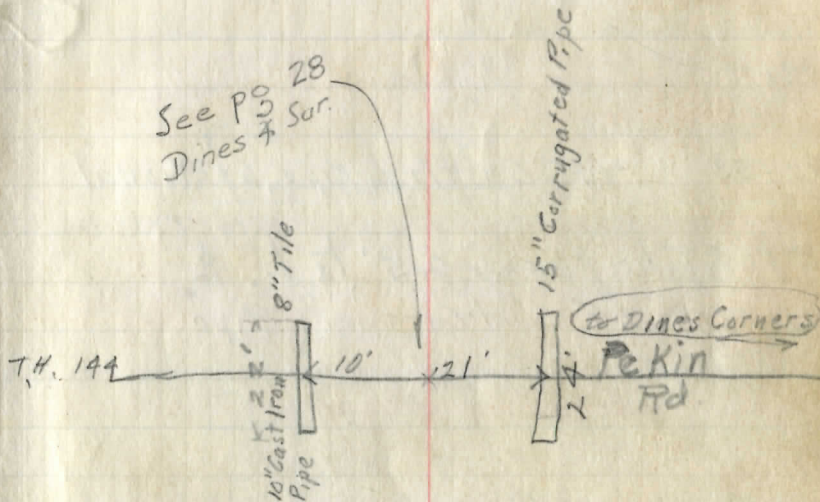
55+89.5 15" Corr. l. Pipe

52+98

78+03 43' Page ③  
77+44 B 77+76 H 77+20



See P<sup>o</sup> 28  
Dines & Sur.



99+99

83  
83  
83

97+00

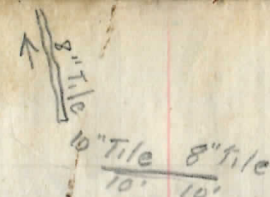
92+53 16" Cast Iron Pipe, Sectional

90 Stake found 25' to L. &  
89+430 24" Solid Cast Iron Pipe

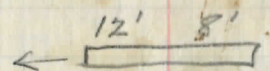
85 stake found 25' to L.

83+00 P.O.T. stake 25' to R. &

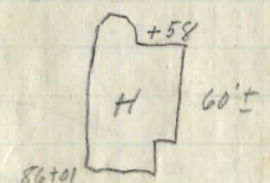
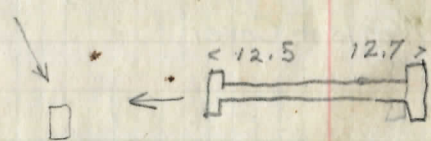
79+76 12" Corr. Iron Pipe, Rusted out



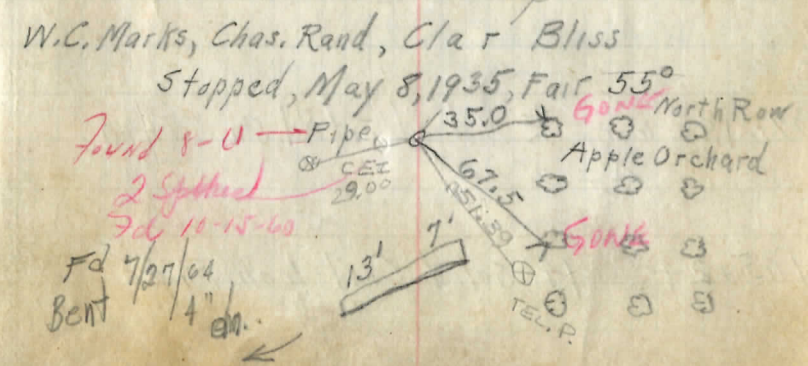
spike 15' x



out house

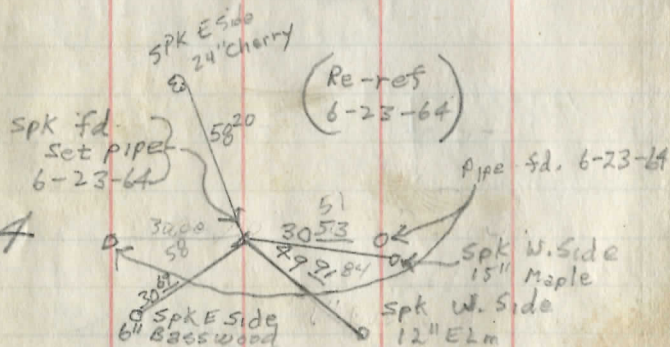


S-W corner in Lamp Post





Cedar Rd



142+59.4

141+39

2 1/2 Wide 2 1/4 Deep

stone Walls fair Conc. Slab + H.W. good

140 Stake 25' L. E - N side drive to W.

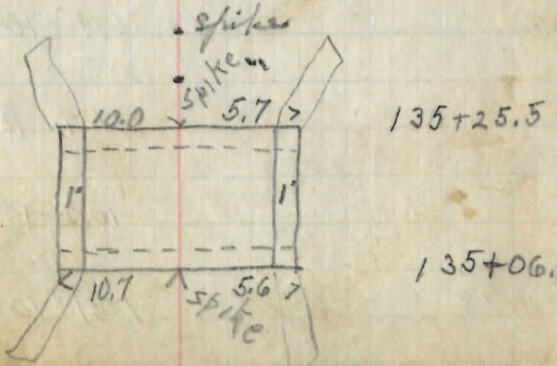
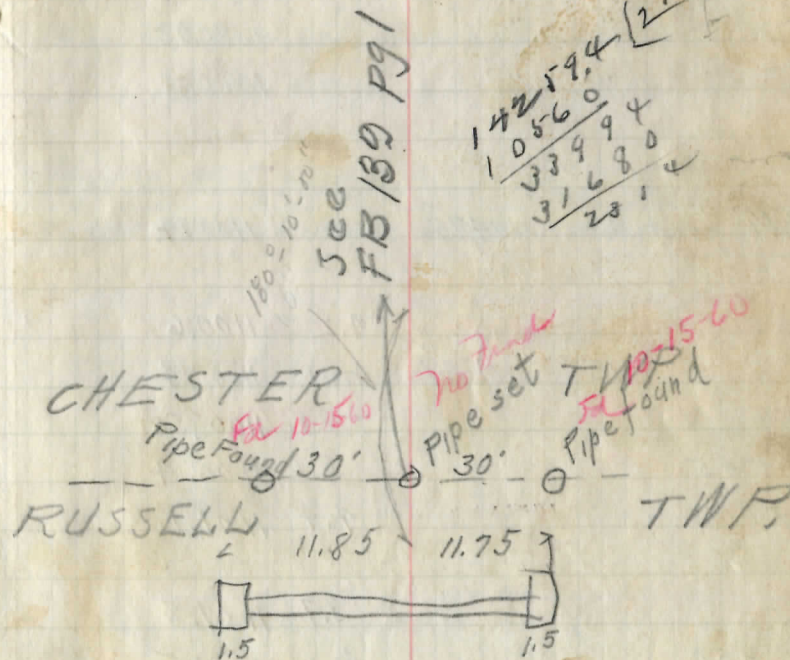
" " " " near Tel. pole

Bridge, stone Walls, good  
 Concrete deck, fair.  
 Span, Top, 16', Batter 1/2  
 Stake 25' L. E / 15' S, if avail.

MON. box

142+59.4  
 10560  
 33994  
 31680  
 2812

12.64



B.M. on N. Woodland

1074.76

" " " " "

1058.30

" " " Route 87

1100.74 sperry, 2 1/5

" " "

1100.70

" " "

1080.05

1095.58

B.M 4.01 1104.75

1100.74

0+00

4.2 1100.6

4.75 1105.49

4.01 1100.74

0+00

4.93 1100.56

0+45

5.1 1100.4

1+00

4.4 1101.1

2

3.7 1101.8

+50

4.0 1101.5

3

6.4 1099.1

4

9.4 1096.1

5

10.2 1095.3

+78

10.1 1095.4

Spike, S. side, 24" Hickory, 26' h. of 64+53

W. root, 30' Ash, 45' R 40+10

34 Spike in S.E. Root, 15" Maple, h., 19+40, School lot. Hanna, May 29, 1923

X on N.E. Cor., Left Headwall, 8+28 (1923)

Spike, W. Root 24" Maple, 25' R., Sta. 0-5, E Rd. to Chag Falls.

May 10, 1935, Fair, 60° W.C. Marks, Clair Bliss Chas. Rand

Spike, S.E. Root, Maple, h., 19+40, N. Kinsman, (R. 87)

1097.9 1099.5 1100.1 1100.6 1100.1 1098.0 1096.3

6.9 5.3 4.1 4.2 4.7 6.8 8.5

16+00 17+00 18+00 18+69 19+00 20+00 21+00

stations on R. 87

1.9 2.8 5.3 5.0 4.4 5.4 4.1 3.7  
25 11.5 12.5 10 0 10 13.5 25

2.2 2.7 4.8 4.1 3.7 4.4 4.8 4.1 3.7 4.1  
25 16 11.8 9 0 9 10 12 18 25

4.0 3.9 7.3 6.7 6.4 7.0 8.0 4.3 3.4  
25 15.5 11-7.5 8 0 8 10.4 16 25

9.2 9.7 10.4 10.2 9.7 10.0 9.4 9.0  
25 13 11.5 9.5 0 8 17 25

11.1 11.4 10.8 10.2 10.7 10.6 10.4  
25-12.5 11 8 0 8 20 25

1088.7 1092.0 1092.4 1095.4 1093.4 1094.7

16.8 13.5 13.1 10.1 12.1 10.8

100 25 10 0 F.L. 80

F.L.

10

6

1105.49

4.16

1099.07

10.2

1095.3

10.58

1094.91

7

+80

3.6

1095.5

1.8

1097.3

8

2.2

1096.9

9

5.1

1094.0

10

6.2

1092.9

11

7.7

1091.4

12

11.7

1087.4

1.00

1087.08

12.99

1086.08

13

6.4

1080.7

14

11.2

1075.9

3.95

1080.13

10.90

1076.18

15

5.8

1074.3

15+61

6.6

1073.5

16

6.7

1073.4

$$\frac{12.3}{2.5} \quad \frac{11.3}{13} \quad \frac{4.5}{11} \quad \frac{10.8}{9} \quad \frac{10.2}{0} \quad \frac{10.4}{7} \quad \frac{11.3}{11} \quad \frac{11.0}{2.5}$$

$$\frac{2.8}{2.5} \quad \frac{3.2}{16.5} \quad \frac{4.8}{12} \quad \frac{4.2}{10} \quad \frac{3.6}{0} \quad \frac{3.8}{5} \quad \frac{3.2}{15} \quad \frac{2.0}{2.5}$$

$$\frac{1.3}{2.5} \quad \frac{1.2}{19.5} \quad \frac{2.5}{13.5} \quad \frac{3.2}{12} \quad \frac{2.2}{0} \quad \frac{2.7}{6} \quad \frac{1.6}{11} \quad \frac{0.0}{2.5}$$

$$\frac{5.0}{2.5} \quad \frac{4.5}{2.0} \quad \frac{5.0}{12} \quad \frac{5.6}{11} \quad \frac{5.0}{7} \quad \frac{5.1}{0} \quad \frac{5.6}{7} \quad \frac{4.9}{9} \quad \frac{4.3}{2.5}$$

$$\frac{7.0}{2.5} \quad \frac{6.6}{12} \quad \frac{6.9}{11} \quad \frac{6.3}{6} \quad \frac{6.2}{0} \quad \frac{7.0}{7} \quad \frac{7.3}{8} \quad \frac{6.2}{9} \quad \frac{5.2}{2.5}$$

$$\frac{7.4}{2.5-13} \quad \frac{8.7}{11} \quad \frac{8.0}{6} \quad \frac{7.7}{0} \quad \frac{8.4}{7} \quad \frac{9.4}{8} \quad \frac{5.8}{14} \quad \frac{5.3}{2.5}$$

$$\frac{9.5}{2.5} \quad \frac{9.2}{14} \quad \frac{12.6}{10} \quad \frac{12.0}{8} \quad \frac{11.7}{0} \quad \frac{12.3}{9} \quad \frac{12.8}{12} \quad \frac{7.4}{23} \quad \frac{6.7}{2.5}$$

$$\frac{3.3}{2.5} \quad \frac{3.6}{17} \quad \frac{7.5}{12} \quad \frac{6.7}{10} \quad \frac{6.4}{0} \quad \frac{7.5}{8} \quad \frac{0.6}{20} \quad \frac{0.0}{2.5}$$

$$\frac{9.7}{2.5} \quad \frac{10.3}{18} \quad \frac{11.7}{13} \quad \frac{10.9}{5} \quad \frac{11.2}{0} \quad \frac{11.7}{6} \quad \frac{7.8}{16} \quad \frac{7.0}{2.5}$$

$$\frac{7.0}{2.5} \quad \frac{6.4}{15} \quad \frac{5.4}{4} \quad \frac{5.8}{0} \quad \frac{6.3}{5} \quad \frac{6.4}{2.5}$$

$$\begin{matrix} 1068.1 & 1070.0 & 1070.2 \\ 12.0 & 10.1 & 9.9 \\ 6.0 & 2.5 & 17.7 \\ & & F.L. \end{matrix} \quad \begin{matrix} 1073.5 \\ 6.6 \\ 0 \\ 6.7 \\ 0 \end{matrix} \quad \begin{matrix} 1071.2 \\ 8.9 \\ 6.3 \\ F.L. \end{matrix} \quad \begin{matrix} 1072.6 \\ 7.5 \\ 30 \end{matrix}$$

$$\frac{8.3}{2.5} \quad \frac{7.5}{15} \quad \frac{6.5}{4} \quad \frac{6.7}{0} \quad \frac{7.8}{6} \quad \frac{7.1}{2.5}$$

1080.3 ✓

17 6.3 1073.8

18 3.8 1076.3

19 5.1 1075.0

+48.3 4.9 1075.2

20 5.0 1075.1

21 4.8 1075.3

1.98 1073.51 8.60 1071.53

22 2.6 1070.9

23 6.5 1067.0

24 8.8 1064.7

+97.5 9.7 1063.8

25 9.6 1063.9

26 9.8 1063.7

+20 9.6 1063.9

$$\begin{array}{r} 4.6 \\ 25 \end{array} \quad \begin{array}{r} 4.9 \\ 19 \end{array} \quad \begin{array}{r} 7.3 \\ 15 \end{array} \quad \begin{array}{r} 6.6 \\ 12 \end{array} \quad \begin{array}{r} 6.0 \\ 5 \end{array} \quad \begin{array}{r} 6.3 \\ 0 \end{array} \quad \begin{array}{r} 6.9 \\ 6 \end{array} \quad \begin{array}{r} 5.1 \\ 10 \end{array} \quad \begin{array}{r} 2.5 \\ 25 \end{array}$$

$$\begin{array}{r} 2.9 \\ 25 \end{array} \quad \begin{array}{r} 3.0 \\ 18 \end{array} \quad \begin{array}{r} 4.7 \\ 15 \end{array} \quad \begin{array}{r} 4.1 \\ 13 \end{array} \quad \begin{array}{r} 3.3 \\ 4 \end{array} \quad \begin{array}{r} 3.8 \\ 0 \end{array} \quad \begin{array}{r} 4.8 \\ 6 \end{array} \quad \begin{array}{r} 2.6 \\ 10 \end{array} \quad \begin{array}{r} 1.2 \\ 18 \end{array} \quad \begin{array}{r} 0.8 \\ 25 \end{array}$$

$$\begin{array}{r} 5.3 \\ 25 \end{array} \quad \begin{array}{r} 5.7 \\ 15 \end{array} \quad \begin{array}{r} 5.2 \\ 11 \end{array} \quad \begin{array}{r} 4.7 \\ 6 \end{array} \quad \begin{array}{r} 5.1 \\ 0 \end{array} \quad \begin{array}{r} 5.7 \\ 7 \end{array} \quad \begin{array}{r} 4.8 \\ 9 \end{array} \quad \begin{array}{r} 3.8 \\ 25 \end{array}$$

1070.4      1073.2

$$\begin{array}{r} 9.7 \\ 75 \end{array} \quad \begin{array}{r} 6.9 \\ 14.0 \\ FL \end{array} \quad \begin{array}{r} 1075.2 \\ 4.9 \\ 0 \end{array} \quad \begin{array}{r} 1073.5 \\ 6.6 \\ 6.1 \\ FL \end{array} \quad \begin{array}{r} 1075.8 \\ 4.3 \\ 3.0 \end{array}$$

$$\begin{array}{r} 6.6 \\ 25 \end{array} \quad \begin{array}{r} 5.4 \\ 14 \end{array} \quad \begin{array}{r} 5.6 \\ 12 \end{array} \quad \begin{array}{r} 5.0 \\ 4 \end{array} \quad \begin{array}{r} 5.0 \\ 0 \end{array} \quad \begin{array}{r} 5.3 \\ 5 \end{array} \quad \begin{array}{r} 5.9 \\ 8 \end{array} \quad \begin{array}{r} 5.1 \\ 10 \end{array} \quad \begin{array}{r} 4.2 \\ 25 \end{array}$$

$$\begin{array}{r} 4.3 \\ 25 \end{array} \quad \begin{array}{r} 4.5 \\ 15 \end{array} \quad \begin{array}{r} 5.9 \\ 12 \end{array} \quad \begin{array}{r} 5.4 \\ 10 \end{array} \quad \begin{array}{r} 4.8 \\ 3 \end{array} \quad \begin{array}{r} 4.8 \\ 0 \end{array} \quad \begin{array}{r} 5.4 \\ 6 \end{array} \quad \begin{array}{r} 6.1 \\ 9 \end{array} \quad \begin{array}{r} 4.7 \\ 11 \end{array} \quad \begin{array}{r} 2.9 \\ 21 \end{array} \quad \begin{array}{r} 2.3 \\ 25 \end{array}$$

$$\begin{array}{r} 0.4 \\ 25 \end{array} \quad \begin{array}{r} 1.2 \\ 15 \end{array} \quad \begin{array}{r} 3.5 \\ 11 \end{array} \quad \begin{array}{r} 3.2 \\ 8 \end{array} \quad \begin{array}{r} 2.6 \\ 0 \end{array} \quad \begin{array}{r} 3.1 \\ 6 \end{array} \quad \begin{array}{r} 4.0 \\ 9 \end{array} \quad \begin{array}{r} 1.1 \\ 13 \end{array} \quad \begin{array}{r} 0.0 \\ 25 \end{array}$$

$$\begin{array}{r} 3.4 \\ 25 \end{array} \quad \begin{array}{r} 3.8 \\ 17 \end{array} \quad \begin{array}{r} 7.3 \\ 10 \end{array} \quad \begin{array}{r} 6.9 \\ 6 \end{array} \quad \begin{array}{r} 6.5 \\ 0 \end{array} \quad \begin{array}{r} 7.1 \\ 8 \end{array} \quad \begin{array}{r} 7.3 \\ 10 \end{array} \quad \begin{array}{r} 5.7 \\ 15 \end{array} \quad \begin{array}{r} 4.6 \\ 25 \end{array}$$

$$\begin{array}{r} 8.7 \\ 25 \end{array} \quad \begin{array}{r} 9.5 \\ 15 \end{array} \quad \begin{array}{r} 9.2 \\ 11 \end{array} \quad \begin{array}{r} 9.2 \\ 7 \end{array} \quad \begin{array}{r} 8.8 \\ 0 \end{array} \quad \begin{array}{r} 9.4 \\ 6 \end{array} \quad \begin{array}{r} 10 \\ 10 \end{array} \quad \begin{array}{r} 8.8 \\ 25 \end{array}$$

1059.1      1060.5

$$\begin{array}{r} 14.4 \\ 50 \end{array} \quad \begin{array}{r} 13.0 \\ 12 \end{array} \quad \begin{array}{r} 9.3 \\ 3 \end{array} \text{ stocked} \quad \begin{array}{r} 1063.8 \\ 9.7 \end{array} \quad \begin{array}{r} 1060.9 \\ 12.6 \\ 11 FL \end{array} \quad \begin{array}{r} 1062.9 \\ 10.6 \\ 2.5 \end{array}$$

$$\begin{array}{r} 12.5 \\ 25 \end{array} \quad \begin{array}{r} 11.7 \\ 11 \end{array} \quad \begin{array}{r} 10.2 \\ 7 \end{array} \quad \begin{array}{r} 9.6 \\ 0 \end{array} \quad \begin{array}{r} 10.0 \\ 8 \end{array} \quad \begin{array}{r} 11.8 \\ 13 \end{array} \quad \begin{array}{r} 10.9 \\ 15 \end{array} \quad \begin{array}{r} 10.6 \\ 25 \end{array}$$

$$\begin{array}{r} 9.8 \\ 25 \end{array} \quad \begin{array}{r} 10.0 \\ 9 \end{array} \quad \begin{array}{r} 9.8 \\ 0 \end{array} \quad \begin{array}{r} 10.0 \\ 12 \end{array} \quad \begin{array}{r} 9.5 \\ 25 \end{array}$$

1073.51 ✓  
 1.78 1063.08 ✓

27 4.5 1058.6

28 9.5 1053.6

B.M. set, 1.19 1052.54 ✓ 11.73 1051.35 ✓

29 2.7 1049.8

30 4.7 1047.8

31 6.0 1046.5

32 6.0 1046.5

+14.3 5.5 1047.0

33 3.4 1049.1

8.47 1059.91 ✓ 1.10 1051.44 ✓

34 5.7 1054.2

+60 2.0 1057.9

35 1.8 1058.1

36 2.2 1057.7

$\frac{1.2}{2.5} \frac{2.2}{11} \frac{5.0}{7} \quad \frac{4.5}{0} \frac{4.8}{8} \frac{5.0}{12} \frac{1.3}{17} \frac{0.6}{25}$

$\frac{7.2}{2.5} \frac{8.1}{10} \frac{9.9}{7} \quad \frac{9.5}{6} \frac{9.4}{4} \frac{10.1}{13} \frac{7.7}{19} \frac{6.7}{2.5}$

2' above ground.  
 Spike <sub>N</sub> E. side, W. cherry, 30'L, sta. 29+97

$\frac{2.2}{2.5} \frac{2.0}{10} \frac{3.0}{7} \quad \frac{2.7}{0} \frac{2.7}{10} \frac{3.4}{12} \frac{0.5}{22} \frac{0.2}{2.5}$

$\frac{3.8}{2.5} \frac{4.5}{11} \frac{5.6}{8} \frac{5.1}{5} \quad \frac{4.7}{0} \frac{5.0}{10} \frac{5.9}{18} \frac{2.9}{2.5}$

$\frac{7.8}{2.5} \frac{7.6}{15} \quad \frac{6.0}{0} \frac{6.5}{17} \frac{6.8}{2.5}$

$\frac{8.6}{2.5} \quad \frac{7.7}{10} \frac{6.1}{5} \quad \frac{6.0}{0} \frac{6.2}{10} \frac{8.2}{15} \frac{7.7}{2.5}$   
 1042.7 1043.1 1045.2 1048.5  
 $\frac{9.8}{100} \frac{9.4-7.3-4.0}{10.4} \quad \frac{1047.0}{5.5} \frac{1048.3}{4.2-6.8-9.4} \frac{1043.1}{14.3} \frac{1044.0}{8.5} \frac{30}{30}$

$\frac{4.1}{2.5} \frac{3.7}{10} \quad \frac{3.4}{0} \frac{3.7}{10} \frac{3.2}{2.5}$

$\frac{2.0}{30} \frac{1.5}{17} \frac{6.2}{11} \quad \frac{5.7}{0} \frac{6.0}{9} \frac{2.8}{13} \frac{1.5}{30}$

$\frac{3.1}{2.5} \frac{2.3}{13} \frac{2.7}{11} \quad \frac{1.8}{0} \frac{2.7}{9} \frac{1.4}{12} \frac{0.1}{2.5}$

$\frac{3.028}{2.5} \frac{3.2}{12} \frac{3.5}{11} \frac{2.7}{9} \quad \frac{2.2}{0} \frac{3.0}{9} \frac{2.2}{12} \frac{2.1}{2.5}$

1059.91 ✓  
4.09 1059.77 ✓

37 3.1 1056.7

38 5.6 1054.2

38+96.5 6.1 1053.7

39 6.1 1053.7

40 5.9 1053.9

+60 5.0 1054.8

41 6.0 1053.8

42 8.7 1051.1

42+96.5 9.1 1050.7

43 9.2 1050.6

44 8.0 1051.8

+50 6.8 1053.0

45 8.8 1051.0

$\frac{2.0}{2.5} \frac{1.7}{17} \frac{4.2}{12} \frac{3.8}{8}$

$\frac{3.1}{0} \frac{4.4}{9} \frac{3.3}{12} \frac{2.1}{2.5}$

$\frac{3.4}{2.5} \frac{4.1}{15} \frac{6.2}{10} \frac{6.0}{8}$

$\frac{5.6}{0} \frac{6.1}{8} \frac{5.5}{2.5}$

$\frac{1049.3}{10.5}$   
60

$\frac{1051.8}{8.0}$   
10

$\frac{1053.7}{6.1}$   
0

$\frac{1051.6}{8.2}$   
10

$\frac{1053.6}{6.2}$   
2.5

$\frac{8.1}{2.5} \frac{7.9}{11} \frac{6.6}{7}$

$\frac{6.1}{0} \frac{6.2}{9} \frac{7.5}{13} \frac{6.2}{2.5}$

$\frac{7.1}{2.5} \frac{6.9}{8}$

$\frac{5.9}{0} \frac{6.4}{9} \frac{5.8}{11} \frac{5.0}{2.5}$

$\frac{5.4}{2.5} \frac{5.3}{15} \frac{7.3}{9} \frac{6.8}{7}$

$\frac{6.0}{0} \frac{6.8}{6} \frac{7.1}{11} \frac{6.4}{12} \frac{5.2}{2.5}$

$\frac{8.6}{2.5} \frac{8.7}{15} \frac{9.8}{9} \frac{9.5}{6}$

$\frac{8.7}{0} \frac{9.3}{10} \frac{8.7}{12} \frac{8.3}{2.5}$

1046.2

1048.2

1047.8

1050.7

1048.2

1049.4

$\frac{13.6}{100}$

$\frac{11.6}{15}$

$\frac{12.0}{6.5 \text{ FL}}$

$\frac{9.1}{0}$

$\frac{11.6}{12.0}$

$\frac{10.4}{2.5}$

100

15

6.5 FL

0

F.L.

2.5

$\frac{10.7}{2.5} \frac{10.2}{12} \frac{10.8}{10} \frac{9.6}{6}$

$\frac{9.2}{0} \frac{9.8}{11} \frac{11.1}{13} \frac{10.2}{15} \frac{10.2}{2.5}$

$\frac{6.0}{2.5} \frac{6.7}{15} \frac{8.2}{10}$

$\frac{8.0}{0} \frac{8.3}{9} \frac{8.7}{10} \frac{8.2}{12} \frac{7.7}{2.5}$

$\frac{4.2}{2.5} \frac{4.9}{13} \frac{7.7}{8}$

$\frac{6.8}{0} \frac{7.6}{11} \frac{6.7}{13} \frac{6.2}{2.5}$

$\frac{5.5}{2.5-16} \frac{9.5}{9} \frac{9.2}{5}$

$\frac{8.8}{0} \frac{9.2}{8} \frac{9.9}{12} \frac{8.9}{13} \frac{7.8}{2.5}$

1059.77 ✓

4.65 1052.80 ✓ 11.62 1048.15 ✓

46 4.65 1052.80 6.2 1046.6

+91 " 6.7 1046.1

47 6.9 1045.9

48 6.3 1046.5

+80 2.9 1049.9

49 3.2 1049.6

50 5.8 1047.0

51 8.0 1044.8

6.40 1050.43 ✓ 8.77 1044.03 ✓

52 7.7 1042.7

+98 8.3 1042.1

53 8.3 1042.1

54 6.5 1043.9

+60 3.2 1047.2

55 3.9 1046.5

$\frac{4.5}{25}$	$\frac{5.1}{15}$	$\frac{6.9}{9}$	$\frac{6.5}{4}$	$\frac{6.2}{0}$	$\frac{6.7}{8}$	$\frac{6.3}{2.5}$
1041.4	1043.3	1043.5	1043.4	1046.1	1043.6	1044.5
$\frac{11.4}{200}$	$\frac{9.5}{80}$	$\frac{9.3}{30}$	$\frac{9.4}{11}$	6.7	$\frac{9.2}{8}$	$\frac{8.3}{30}$
						$\frac{1045.2}{7.6}{7.5}$

$\frac{8.4}{25}$	$\frac{7.9}{15}$	$\frac{7.2}{8}$	$\frac{6.9}{0}$	$\frac{7.2}{7}$	$\frac{8.3}{10}$	$\frac{7.6}{14}$	$\frac{7.5}{2.5}$
------------------	------------------	-----------------	-----------------	-----------------	------------------	------------------	-------------------

$\frac{4.6}{25}$	$\frac{5.5}{12}$	$\frac{6.9}{10}$	$\frac{6.3}{0}$	$\frac{6.8}{7}$	$\frac{5.6}{10}$	$\frac{4.2}{2.5}$
------------------	------------------	------------------	-----------------	-----------------	------------------	-------------------

$\frac{1.6}{25}$	$\frac{2.5}{12}$	$\frac{4.0}{10}$	$\frac{3.2}{0}$	$\frac{3.9}{7}$	$\frac{2.7}{10}$	$\frac{1.9}{2.5}$
------------------	------------------	------------------	-----------------	-----------------	------------------	-------------------

$\frac{3.4}{25}$	$\frac{4.3}{15}$	$\frac{6.4}{11}$	$\frac{5.8}{0}$	$\frac{6.3}{6}$	$\frac{5.5}{10}$	$\frac{5.3}{2.5}$
------------------	------------------	------------------	-----------------	-----------------	------------------	-------------------

$\frac{7.1}{25}$	$\frac{7.7}{12}$	$\frac{8.9}{10}$	$\frac{8.0}{0}$	$\frac{8.2}{4}$	$\frac{8.5}{5}$	$\frac{8.6}{9}$	$\frac{7.2}{12}$	$\frac{5.8}{2.5}$
------------------	------------------	------------------	-----------------	-----------------	-----------------	-----------------	------------------	-------------------

$\frac{6.7}{25}$	$\frac{7.2}{12}$	$\frac{8.3}{9}$	$\frac{7.7}{0}$	$\frac{8.3}{7}$	$\frac{7.1}{13}$	$\frac{6.5}{2.5}$
------------------	------------------	-----------------	-----------------	-----------------	------------------	-------------------

1038.1	1039.8	1042.1	1040.0	1041.9
$\frac{12.3}{100}$	$\frac{10.6}{9}$	$\frac{8.3}{0}$	$\frac{10.4}{7}$	$\frac{8.5}{2.5}$

$\frac{10.1}{25}$	$\frac{8.3}{0}$	$\frac{8.5}{2.5}$
-------------------	-----------------	-------------------

$\frac{4.3}{25}$	$\frac{4.6}{14}$	$\frac{7.0}{9}$	$\frac{6.5}{0}$	$\frac{7.1}{7}$	$\frac{5.7}{9}$	$\frac{3.3}{2.5}$
------------------	------------------	-----------------	-----------------	-----------------	-----------------	-------------------

$\frac{2.2}{25}$	$\frac{2.6}{12}$	$\frac{3.7}{10}$	$\frac{3.2}{0}$	$\frac{3.9}{8}$	$\frac{2.2}{10}$	$\frac{0.3}{2.5}$
------------------	------------------	------------------	-----------------	-----------------	------------------	-------------------

$\frac{3.2}{25}$	$\frac{3.5}{11}$	$\frac{4.7}{10}$	$\frac{3.9}{0}$	$\frac{4.6}{8}$	$\frac{3.3}{10}$	$\frac{1.6}{2.5}$
------------------	------------------	------------------	-----------------	-----------------	------------------	-------------------

1050.43 ✓  
 55+89.5 5.2 1045.2  
 56 " 5.2 1045.2  
 57 4.1 1046.3 ✓  
 2.23 1055.49 ✓ 2.17 1048.26  
 B.M, set 2.03 1053.46 ✓

B.M 0.61 1054.07 ✓ 1053.46 ✓  
 58 3.7 1050.4  
 +5.0 1.9 1052.2  
 59 2.3 1051.8  
 60 7.4 1046.7  
 61 14.0 1040.1 ✓  
 0.72 1038.46 ✓ 16.33 1037.74  
 62 4.0 1034.5  
 63 8.4 1030.1  
 63+16 9.2 1029.3 ✓  
 0.93 1029.3 2 10.07 1028.39

1040.3 1042.3 1045.2 1042.5 1044.9  
 $\frac{10.1}{100}$   $\frac{8.1}{9.5 F.L.}$   $\frac{5.2}{0}$   $\frac{7.9}{10.5 F.L.}$   $\frac{5.5}{30}$   
 $\frac{7.8}{2.5}$   $\frac{6.1}{11}$   $\frac{5.2}{0}$   $\frac{5.5}{7}$   $\frac{6.7}{11}$   $\frac{6.3}{2.5}$   
 $\frac{2.5}{2.5}$   $\frac{3.6}{1.5}$   $\frac{4.9}{11}$   $\frac{4.1}{0}$   $\frac{4.8}{9}$   $\frac{3.3}{12}$   $\frac{1.5}{2.5}$

R.P. spike, S.W. Root 24" Buckeye, 59+01, Left 20'

May 11, 1934, Fair, 55°, Marks, Bliss, Rand

$\frac{1.2}{2.5}$   $\frac{3.3}{1.5}$   $\frac{4.7}{1.3}$   $\frac{3.7}{0}$   $\frac{4.7}{8}$   $\frac{1.8}{12}$   $\frac{+0.3}{2.5}$   
 $\frac{1.2}{2.5}$   $\frac{1.7}{1.3}$   $\frac{3.5}{1.2}$   $\frac{2.7}{9}$   $\frac{2.3}{0}$   $\frac{2.8}{7}$   $\frac{3.6}{16}$   $\frac{1.2}{1.3}$   $\frac{0.4}{2.5}$   
 $\frac{3.4}{2.5}$   $\frac{4.5}{1.5}$   $\frac{8.0}{10}$   $\frac{7.4}{0}$   $\frac{8.2}{9}$   $\frac{6.2}{12}$   $\frac{5.0}{17}$   $\frac{4.6}{2.5}$   
 $\frac{9.1}{2.5}$   $\frac{10.4}{1.5}$   $\frac{15.9}{9}$   $\frac{14.4}{4}$   $\frac{14.0}{0}$   $\frac{14.6}{9}$   $\frac{15.2}{12}$   $\frac{12.9}{15}$   $\frac{11.1}{2.5}$   
 $\frac{+0.2}{2.5}$   $\frac{1.0}{1.5}$   $\frac{5.1}{7}$   $\frac{5.2}{5}$   $\frac{4.5}{4}$   $\frac{4.0}{0}$   $\frac{3.8}{6}$   $\frac{5.2}{14}$   $\frac{3.8}{16}$   $\frac{2.6}{2.5}$   
 $\frac{6.5}{2.5}$   $\frac{7.1}{1.5}$   $\frac{9.2}{10}$   $\frac{8.7}{7}$   $\frac{8.4}{5}$   $\frac{8.4}{0}$   $\frac{8.4}{10}$   $\frac{9.0}{14}$   $\frac{9.9}{16}$   $\frac{7.5}{2.5}$   
 1035.5 1034.5 1033.3 1032.0  
 $\frac{3.0}{200}$   $\frac{4.0}{150}$   $\frac{5.1}{100}$   $\frac{6.5}{50}$  1029.3 1030.2 1030.8 1031.5 1032.5  
 $\frac{9.2}{0}$   $\frac{8.3}{50}$   $\frac{7.7}{100}$   $\frac{7.0}{150}$   $\frac{6.0}{200}$

1029.32 ✓

64 2.8 1026.5

65 4.1 1025.2

+92.5 4.3 1025.0

66 4.5 1024.8

67 4.8 1024.5

68 4.1 1025.2

69 2.5 1026.8 ✓

15.50 1044.27 ✓ 0.55 1028.77

70 15.2 1029.1

71 9.0 1035.3

72 5.1 1039.2

73 2.6 1041.7 ✓

16.55 1060.68 ✓ 0.14 1044.13

74 16.0 1044.7

$\frac{1.4}{2.5} \frac{2.5}{11} \frac{3.3}{8} \frac{2.6}{6} \frac{2.8}{2.8} \frac{2.8}{9} \frac{2.8}{9} \frac{3.5}{14} \frac{3.1}{15} \frac{3.2}{2.5}$

$\frac{5.5}{2.5} \frac{3.9}{8} \frac{4.4}{2}$   
 $\frac{9.0}{200} \frac{8.2}{100} \frac{7.0}{30} \frac{7.2}{9.7}$   
 $\frac{4.1}{0} \frac{3.6}{6} \frac{4.3}{13} \frac{4.8}{2.5}$   
 $\frac{1020.3}{1025.0} \frac{1021.1}{1026.3} \frac{1022.3}{1022.1} \frac{1022.1}{1022.1} \frac{1022.1}{1022.1} \frac{1022.1}{1022.1} \frac{1022.1}{1022.1} \frac{1022.1}{1022.1} \frac{1022.1}{1022.1} \frac{1022.1}{1022.1}$   
 $\frac{4.3}{0} \frac{3.0}{14.3} \frac{5.6}{7.2} \frac{6.7}{30}$

$\frac{5.7}{2.5} \frac{6.4}{1.5} \frac{5.2}{11} \frac{4.5}{4} \frac{4.5}{0} \frac{4.2}{4} \frac{4.9}{11} \frac{6.3}{17} \frac{5.3}{2.5}$

$\frac{6.2}{2.5} \frac{6.0}{14} \frac{5.0}{8} \frac{5.4}{4} \frac{4.8}{0} \frac{4.4}{4} \frac{5.5}{2.5}$

$\frac{4.9}{2.5} \frac{4.4}{7} \frac{4.6}{3} \frac{4.1}{0} \frac{3.8}{3} \frac{4.4}{9} \frac{5.0}{2.5}$

$\frac{3.1}{2.5} \frac{3.4}{8} \frac{2.5}{0} \frac{2.5}{4} \frac{2.9}{15} \frac{+1.0}{2.5}$

$\frac{15.7}{2.5} \frac{15.3}{12} \frac{15.9}{9} \frac{15.2}{0} \frac{15.2}{9} \frac{15.9}{11} \frac{10.4}{2.5}$

$\frac{5.0}{30} \frac{4.6}{15} \frac{9.8}{8.5} \frac{9.3}{5} \frac{9.0}{0} \frac{9.7}{6} \frac{10.9}{10} \frac{2.7}{2.4} \frac{2.6}{30}$

$\frac{5.7}{2.5} \frac{5.3}{15} \frac{4.4}{9} \frac{5.7}{7} \frac{5.1}{0} \frac{5.2}{9} \frac{5.6}{11} \frac{4.0}{14} \frac{3.6}{2.5}$

$\frac{2.5}{2.5} \frac{3.2}{10} \frac{3.2}{6} \frac{2.6}{0} \frac{3.3}{10} \frac{0.5}{18} \frac{0.0}{20} \frac{+0.5}{2.5}$

$\frac{14.2}{2.5} \frac{14.4}{15} \frac{16.8}{9} \frac{16.0}{0} \frac{17.3}{7} \frac{12.7}{15} \frac{12.0}{2.5}$

✓  
1060.68

75 12.4 1048.3

76 9.0 1051.7

77 3.5 1057.2

77+80 1.9 1058.8

78 3.1 1057.6

79 5.0 1055.7

+76 5.4 1055.3

11.19 1067.87 ✓

80 12.4 1055.5

81 10.7 1057.2

82 8.3 1059.6

83 4.8 1063.1

B.M. set 1.85 1066.02 ✓

$\frac{13.1}{25} \quad \frac{12.6}{11} \quad \frac{13.2}{9}$

$\frac{12.4}{0} \quad \frac{12.7}{10} \quad \frac{12.1}{2.5}$

$\frac{4.9}{31-25-16} \quad \frac{9.5}{11}$

$\frac{9.0}{0} \quad \frac{9.8}{9} \quad \frac{6.5}{15} \quad \frac{6.5}{2.5}$

$\frac{2.3}{25} \quad \frac{1.8}{15} \quad \frac{4.2}{8}$

$\frac{3.5}{0} \quad \frac{4.1}{6} \quad \frac{1.2}{11} \quad \frac{1.3}{2.5}$

$\frac{1.6}{42} \quad \frac{1.6}{16}$

$\frac{1.9}{0} \quad \frac{1.9}{6} \quad \frac{0.6}{10} \quad \frac{0.2}{2.5}$

$\frac{1.7}{43} \quad \frac{2.5}{19}$

$\frac{3.1}{0} \quad \frac{3.0}{5} \quad \frac{0.8}{11} \quad \frac{0.1}{2.5}$

$\frac{5.2}{25} \quad \frac{5.5}{17} \quad \frac{4.6}{13} \quad \frac{4.6}{5}$

$\frac{5.0}{0} \quad \frac{5.4}{7} \quad \frac{4.6}{9} \quad \frac{3.2}{2.5}$

$\frac{1049.0}{2.00} \quad \frac{1051.7}{4.0} \quad \frac{1051.9}{8.8} \quad \frac{1051.9}{13}$

$\frac{1055.3}{5.4} \quad \frac{1052.0}{8.7} \quad \frac{1055.2}{5.5} \quad \frac{1055.2}{30}$

$\frac{13.8}{25} \quad \frac{12.9}{4}$

$\frac{12.4}{0} \quad \frac{12.6}{4} \quad \frac{12.6}{2.5}$

$\frac{9.7}{25} \quad \frac{10.2}{18} \quad \frac{11.9}{12} \quad \frac{10.7}{0}$

$\frac{11.6}{10} \quad \frac{10.1}{2.5}$

$\frac{6.5}{25} \quad \frac{8.2}{12} \quad \frac{9.6}{10} \quad \frac{8.3}{0}$

$\frac{9.5}{7} \quad \frac{8.7}{12} \quad \frac{7.0}{2.5}$

$\frac{3.7}{25} \quad \frac{5.0}{12} \quad \frac{6.0}{11}$

$\frac{4.8}{0} \quad \frac{5.5}{8} \quad \frac{6.1}{10} \quad \frac{4.6}{14} \quad \frac{3.2}{2.5}$

R.P. Spike, N. side 8" Apple, 35' Right, 83+00

1067.87

84 4.4 1063.5

85 5.2 1062.7

86 5.9 1062.0

87 7.2 1060.7

3.32 1061.17 10.02 1057.85

88 5.2 1056.0

89 7.2 1054.0

+43 6.9 1054.3

90 5.4 1055.8

7.84 1065.69 3.32 1057.85

91 6.4 1059.3

92 7.9 1057.8

+53 7.7 1058.0

93 7.2 1058.5

$\frac{5.0}{2.5}$   $\frac{5.8}{12}$   $\frac{4.8}{8}$   $\frac{4.4}{0}$   $\frac{4.8}{8}$   $\frac{5.2}{11}$   $\frac{3.7}{13}$   $\frac{2.4}{2.5}$

$\frac{5.8}{2.5}$   $\frac{6.0}{13}$   $\frac{6.2}{11}$   $\frac{5.2}{0}$   $\frac{5.7}{10}$   $\frac{4.4}{13}$   $\frac{3.6}{2.5}$

$\frac{4.7}{2.5}$   $\frac{5.6}{14}$   $\frac{6.5}{12}$   $\frac{5.9}{0}$   $\frac{6.8}{9}$   $\frac{2.8}{18}$   $\frac{2.4}{2.5}$

$\frac{6.3}{2.5}$   $\frac{6.7}{15}$   $\frac{7.9}{12}$   $\frac{7.8}{8}$   $\frac{7.2}{0}$   $\frac{8.2}{8}$   $\frac{8.6}{10}$   $\frac{4.3}{19}$   $\frac{2.8}{30}$

$\frac{4.8}{2.5}$   $\frac{5.5}{16}$   $\frac{6.4}{13}$   $\frac{6.0}{9}$   $\frac{5.2}{0}$   $\frac{5.7}{7}$   $\frac{6.4}{9}$   $\frac{2.1}{17}$   $\frac{0.7}{2.5}$   $\frac{0.1}{30}$

$\frac{9.0}{2.5}$   $\frac{7.7}{8}$   $\frac{7.2}{0}$   $\frac{7.5}{9}$   $\frac{8.2}{2.5}$   
1045.3 1048.1 1049.5 1248.4 1050.9 1053.0 1054.3 1053.4 1051.1 1049.1 1052.2  
15.9 13.1 11.7 12.8 - 10.8 - 8.2 6.9 7.8 - 10.1 - 12.1 9.0  
200 100 30 12.5 12.7 30

$\frac{7.1}{2.5}$   $\frac{6.3}{8}$   $\frac{5.4}{0}$   $\frac{5.8}{8}$   $\frac{6.7}{11}$   $\frac{4.6}{2.5}$

$\frac{4.7}{2.5}$   $\frac{5.2}{14}$   $\frac{7.3}{9}$   $\frac{6.4}{0}$   $\frac{7.2}{8}$   $\frac{2.9}{16}$   $\frac{1.9}{2.5}$

$\frac{9.9}{2.5}$   $\frac{8.5}{15}$   $\frac{7.9}{0}$   $\frac{8.5}{9}$   $\frac{7.2}{2.5}$   
1054.0 1056.1 1055.4 1058.0 1055.2± 1058.1  
11.7 9.6 10.3 7.7 10.5± 7.6  
100 30 12 FL. 8 13 Tile from Field 30

$\frac{8.5}{2.5}$   $\frac{7.8}{8}$   $\frac{7.2}{0}$   $\frac{7.9}{8}$   $\frac{7.6}{2.5}$

1065.69 ✓

94 5.6 1060.1

95 2.5 1063.2

871 1074.40 ✓ 0.00 1065.69 ✓

7.2 1067.2

96

97 4.1 1070.3

98 5.0 1069.4

99 5.6 1068.8

99+99 5.9 1068.5

100 5.9 1068.5

101 5.5 1068.9

102 4.2 1070.2 ✓

4.80 1075.85 ✓ 3.35 1071.05

$\frac{3.9}{2.5}$   $\frac{4.8}{12}$   $\frac{6.1}{8}$   $\frac{5.6}{0}$   $\frac{6.0}{9}$   $\frac{5.2}{11}$   $\frac{4.8}{2.5}$

$\frac{0.6}{2.5}$   $\frac{1.0}{14}$   $\frac{3.2}{8}$   $\frac{2.5}{0}$   $\frac{3.0}{7}$   $\frac{1.9}{11}$   $\frac{1.0}{2.5}$

Top of Stake, 25' right, 95+00

$\frac{5.9}{2.5}$   $\frac{6.5}{14}$   $\frac{8.3}{6}$   $\frac{7.2}{0}$   $\frac{7.7}{6}$   $\frac{7.7}{9}$   $\frac{5.7}{13}$   $\frac{5.2}{2.5}$

$\frac{4.9}{2.5}$   $\frac{4.6}{8}$   $\frac{4.1}{0}$   $\frac{4.5}{5}$   $\frac{4.7}{9}$   $\frac{3.4}{11}$   $\frac{3.0}{2.5}$

$\frac{5.1}{2.5}$   $\frac{5.1}{11}$   $\frac{5.5}{9}$   $\frac{5.0}{0}$   $\frac{4.9}{12}$   $\frac{4.0}{2.5}$

1058.2  $\frac{5.8}{2.5}$   $\frac{6.1}{12-7}$   $\frac{5.6}{0}$   $\frac{6.0}{5}$   $\frac{5.7}{2.5}$   
1060.4  $\frac{5.6}{10.6}$   $\frac{1065.7}{8.7}$   $\frac{1066.2}{8.2}$   $\frac{1068.5}{5.9}$   $\frac{1066.5}{7.9}$   $\frac{1066.7}{7.7}$   
400 300 200 100  $\frac{8.7}{12}$   $\frac{10}{10}$  F.L.  $\frac{1}{1}$  F.L.  $\frac{13}{13}$  Tile  $\frac{5.8}{30}$   
Ground, Valley to N.W. Inlet to 8" tile

$\frac{6.9}{2.5}$   $\frac{6.6}{9}$   $\frac{5.9}{0}$   $\frac{6.5}{10}$   $\frac{6.0}{2.5}$

$\frac{6.1}{2.5}$   $\frac{6.0}{8}$   $\frac{5.5}{0}$   $\frac{6.0}{6}$   $\frac{5.4}{9}$   $\frac{4.4}{2.5}$

$\frac{3.9}{2.5}$   $\frac{4.2}{11}$   $\frac{4.9}{10}$   $\frac{4.0}{4}$   $\frac{4.2}{0}$   $\frac{4.8}{7}$   $\frac{2.9}{10}$   $\frac{2.0}{2.5}$

1075.85

102+55 4.0 1076.9

103 4.4 1071.5

104 7.1 1068.8

B.M. Set 5.66 1070.19

105 8.1 1067.8

+24 8.3 1067.6

106 7.7 1068.2

107 6.0 1069.9

107+21.9 5.11 1070.74

107+21.9 5.11 1070.8

108 3.5 1072.4

109 4.3 1071.6

5.00 1074.85 6.00 1069.85

0.44 1074.41

$\frac{4.4}{2.5}$   $\frac{4.2}{12}$   $\frac{4.7}{11}$   $\frac{4.0}{0}$   $\frac{4.6}{7}$   $\frac{2.9}{9}$   $\frac{2.2}{2.5}$

$\frac{4.6}{2.5}$   $\frac{4.7}{12}$   $\frac{5.1}{11}$   $\frac{4.3}{6}$   $\frac{4.4}{0}$   $\frac{5.0}{8}$   $\frac{3.4}{10}$   $\frac{2.9}{2.5}$

$\frac{5.9}{2.5}$   $\frac{6.7}{13}$   $\frac{7.7}{10}$   $\frac{7.1}{0}$   $\frac{7.8}{7}$   $\frac{5.9}{10}$   $\frac{5.1}{2.5}$

Spike E. root, 12" Maple 30'± h. Sta 104+50±

$\frac{9.1}{2.5}$   $\frac{8.4}{10}$   $\frac{8.1}{0}$   $\frac{9.2}{11}$   $\frac{9.0}{2.5}$

1063.0 1064.2 1064.9 1064.4 1067.6 1064.6 1066.3

$\frac{12.9}{140}$   $\frac{11.7}{110}$   $\frac{11.0}{30}$   $\frac{11.5}{15.4}$   $\frac{8.3}{0}$   $\frac{11.3}{9.0}$   $\frac{9.6}{2.5}$

F.L. F.L.

$\frac{8.6}{2.5}$   $\frac{8.1}{14}$   $\frac{8.3}{9}$   $\frac{7.7}{0}$   $\frac{8.2}{5}$   $\frac{8.0}{2.5}$

$\frac{6.2}{2.5}$   $\frac{6.7}{16}$   $\frac{6.0}{0}$   $\frac{7.0}{10}$   $\frac{5.6}{14}$   $\frac{5.0}{2.5}$

Iron Pipe, # N. Woodland

1069.6 1070.2 1070.3 1070.4 1070.7 1070.8 1070.9 1070.9 1070.8 1070.2 1069.6 1069.3

$\frac{6.3}{300}$   $\frac{5.7}{250}$   $\frac{5.6}{200}$   $\frac{5.5}{150}$   $\frac{5.5}{100}$   $\frac{5.15}{50}$   $\frac{5.1}{0}$   $\frac{5.0}{50}$   $\frac{5.0}{100}$   $\frac{5.1}{150}$   $\frac{5.7}{200}$   $\frac{6.3}{250}$   $\frac{6.6}{300}$

$\frac{3.2}{2.5}$   $\frac{3.4}{12}$   $\frac{4.0}{9}$   $\frac{3.5}{0}$   $\frac{4.3}{9}$   $\frac{3.6}{10}$   $\frac{3.0}{2.5}$

$\frac{4.7}{2.5}$   $\frac{4.4}{13}$   $\frac{5.0}{9}$   $\frac{4.3}{0}$   $\frac{4.6}{6}$   $\frac{5.4}{9}$   $\frac{4.1}{10}$   $\frac{3.7}{2.5}$

Spike, S. side, 24" Hickory, N. Woodland, 64+53, 1074.76

2.87 1073.61

1070.74

110 3.6 1070.0

111 4.6 1069.0

112 5.0 1068.6

113 6.3 1067.3

114 9.1 1064.5

115 10.8 1062.8

3.56 1067.09

10.08 1063.53

116 5.1 1062.0

+50

5.4 1061.7

117 5.6 1061.5

118 4.7 1062.4

119 3.3 1063.8

May 13, 1935; Cloudy, Showers, 60° W.C. Marks  
Chas. Rand  
Glen Wilder

Iron Pipe & Cave Rd. + N. Woodland.

$\frac{4.0}{25}$   $\frac{4.3}{9}$   $\frac{3.6}{0}$   $\frac{4.4}{8}$   $\frac{3.4}{10}$   $\frac{2.6}{25}$

$\frac{5.7}{25}$   $\frac{5.3}{8}$   $\frac{4.6}{0}$   $\frac{5.5}{11}$   $\frac{5.1}{25}$

$\frac{5.4}{25}$   $\frac{5.8}{10}$   $\frac{5.0}{0}$   $\frac{5.1}{5}$   $\frac{6.6}{10}$   $\frac{6.0}{11}$   $\frac{5.8}{25}$

$\frac{5.7}{25}$   $\frac{6.2}{12}$   $\frac{7.4}{10}$   $6.3$   $\frac{6.7}{7}$   $\frac{7.5}{10}$   $\frac{6.4}{15}$   $\frac{5.9}{25}$

$\frac{7.9}{25}$   $\frac{8.5}{14}$   $\frac{9.6}{9}$   $\frac{9.1}{0}$   $\frac{10.0}{9}$   $\frac{8.2}{11}$   $\frac{7.4}{25}$

$\frac{10.9}{25}$   $\frac{11.3}{11}$   $\frac{10.8}{8}$   $\frac{11.1}{10}$   $\frac{11.1}{25}$

Top of Stake, 25' R 115 + 00

$\frac{6.1}{25}$   $\frac{5.9}{12}$   $\frac{5.1}{0}$   $\frac{5.4}{5}$   $\frac{6.3}{25}$

1060.9  
 $\frac{6.2}{30}$   
1061.7  
5.4  
0  
1061.4  
5.7  
0  
1060.5  
6.6  
30  
1060.0  
7.1  
100  
1059.7  
7.4  
200  
1058.4  
8.7  
300  
1057.6  
9.5  
400  
9.9  
500  
outlet same for Sta. 117 + 00

$\frac{6.0}{25}$   $\frac{6.0}{9}$   $\frac{5.6}{0}$   $\frac{5.8}{8}$   $\frac{6.4}{25}$

$\frac{4.3}{25}$   $\frac{4.5}{16}$   $\frac{5.2}{12}$   $\frac{4.7}{0}$   $\frac{5.5}{7}$   $\frac{4.7}{9}$   $\frac{4.2}{25}$

$\frac{3.1}{25}$   $\frac{3.9}{13}$   $\frac{2.9}{5}$   $\frac{3.3}{0}$   $\frac{4.0}{5}$   $\frac{3.5}{8}$   $\frac{3.3}{25}$

1067.09

120 4.5 1062.6

121 5.6 1061.5

122 7.5 1059.6

123 10.8 1056.3

0.72 1056.19 11.62 1055.47

124 5.0 1051.2

125 9.2 1047.0

126 11.4 1044.8

127 13.2 1043.0

127+23 13.4 1042.8

128 11.9 1044.3

129 7.3 1048.9

5.70 1060.10 1.79 1054.40

130 4.1 1056.0

$$\frac{4.3}{2.5} \quad \frac{5.0}{13} \quad \frac{4.2}{5} \quad \frac{4.5}{0} \quad \frac{5.3}{6} \quad \frac{4.6}{9} \quad \frac{3.9}{2.5}$$

$$\frac{6.0}{2.5} \quad \frac{6.0}{17} \quad \frac{6.4}{13} \quad \frac{5.6}{5-0} \quad \frac{6.6}{6} \quad \frac{5.3}{10} \quad \frac{4.1}{2.5}$$

$$\frac{7.5}{2.5} \quad \frac{7.2}{14} \quad \frac{8.0}{12} \quad \frac{7.5}{5.0 \ 0} \quad \frac{8.3}{6} \quad \frac{6.3}{10} \quad \frac{5.4}{2.5}$$

$$\frac{8.5}{2.5} \quad \frac{8.6}{15} \quad \frac{11.1}{11} \quad \frac{10.8}{5-0} \quad \frac{12.3}{4} \quad \frac{8.8}{11} \quad \frac{7.9}{2.5}$$

$$\frac{2.2}{2.5} \quad \frac{3.0}{17} \quad \frac{4.8}{11} \quad \frac{5.7}{7} \quad \frac{5.0}{5.0} \quad \frac{5.7}{3} \quad \frac{6.8}{6} \quad \frac{3.5}{12} \quad \frac{2.7}{2.5}$$

$$\frac{8.2}{2.5} \quad \frac{8.1}{15} \quad \frac{10.3}{11} \quad \frac{9.7}{8} \quad \frac{9.1}{3} \quad \frac{9.2}{0} \quad \frac{9.7}{7} \quad \frac{8.6}{12} \quad \frac{8.2}{2.5}$$

$$\frac{11.2}{2.8} \quad \frac{12.0}{11} \quad \frac{11.4}{0} \quad \frac{12.2}{8} \quad \frac{12.0}{2.5}$$

$$\frac{15.5}{2.5} \quad \frac{13.6}{9} \quad \frac{14.7}{7} \quad \frac{13.7}{5} \quad \frac{13.2}{0} \quad \frac{13.6}{6} \quad \frac{14.8}{2.5}$$

$$\begin{array}{r} 1037.2 \\ 19.0 \\ \hline 100 \end{array} \quad \begin{array}{r} 1037.2 \\ 19.0 \\ \hline 100 \end{array} \quad \begin{array}{r} 1040.6 \\ 14.4 \\ \hline 12.0 \end{array} \quad \begin{array}{r} 1041.8 \\ 13.4 \\ \hline 1042.8 \end{array} \quad \begin{array}{r} 1043.4 \\ 12.8 \\ \hline 13.5 \end{array} \quad \begin{array}{r} 1040.6 \\ 15.6 \\ \hline 19.0 \end{array} \quad \begin{array}{r} 1037.2 \\ 19.0 \\ \hline 1042.8 \end{array}$$

$$\frac{14.6}{2.5} \quad \frac{14.1}{15} \quad \frac{12.5}{5} \quad \frac{11.9}{0} \quad \frac{12.2}{8} \quad \frac{13.2}{13} \quad \frac{13.8}{2.5}$$

$$\frac{2.4}{35-28} \quad \frac{4.9}{15} \quad \frac{6.3}{9} \quad \frac{7.8}{6} \quad \frac{7.2}{4} \quad \frac{7.3}{0} \quad \frac{7.7}{12} \quad \frac{5.7}{17} \quad \frac{5.3}{2.5} \quad \frac{5.0}{30}$$

$$\frac{2.2}{30-25-14} \quad \frac{5.3}{9} \quad \frac{4.1}{0} \quad \frac{4.8}{10} \quad \frac{2.9}{13} \quad \frac{2.3}{2.5-30}$$

1060.10

130+50

2.9 1057.2

131

4.0 1056.1

132

6.8 1053.3

+60

9.4 1050.7

16.23 1043.87

133

11.4 1048.7

5.25 1049.12

1043.87

134

4.3 1044.8

135

4.5 1044.6

+16

4.2 1044.9

136

4.4 1044.7

137

4.6 1044.5

138

4.1 1045.0

$\frac{2.4}{2.5} \frac{1.9}{1.5} \frac{3.6}{1.2}$

$\frac{2.9}{0} \frac{3.5}{8} \frac{1.5}{1.2} \frac{1.7}{2.5-30}$

$\frac{2.1}{30-25} \frac{1.7}{17} \frac{4.9}{10}$

$\frac{4.0}{0} \frac{4.6}{5} \frac{0.4}{13} \frac{0.0}{30}$

$\frac{2.7}{30} \frac{2.7}{20} \frac{2.9}{10}$

$\frac{6.8}{0} \frac{7.9}{5} \frac{2.2}{14} \frac{1.8}{30}$

$\frac{1.9}{30} \frac{2.2}{22} \frac{9.9}{10} \frac{9.4}{0} \frac{10.7}{6} \frac{1.8}{2.5-30}$

Spike, E. Side, 15" Elm, 30±L, 133+90

$\frac{16.0}{2.5}$

$\frac{11.6}{9} \frac{12.1}{7}$

$\frac{11.4}{0} \frac{12.0}{7}$

$\frac{11.4}{13} \frac{7.7}{2.5}$

$\frac{7.3}{2.5} \frac{6.5}{1.5} \frac{4.6}{8}$

$\frac{4.3}{0} \frac{4.6}{3} \frac{7.4}{1.5} \frac{7.0}{2.5}$

$\frac{7.6}{2.5} \frac{4.6}{7}$

$\frac{4.5}{0} \frac{4.6}{3} \frac{8.6}{9} \frac{9.0}{2.5}$

1038.1 1037.0 1044.1 1045.9 1044.9  
11.0 12.1 5.0-3.2 4.2 3.2 5.1 9.7 13.7  
100 10.4 5.6 water

$\frac{8.3}{30-17} \frac{4.9}{11}$

$\frac{4.4}{0} \frac{5.0}{7} \frac{8.2}{11-30}$

$\frac{8.4}{30} \frac{4.6}{8}$

$\frac{5.0}{6} \frac{7.3}{11-30}$

$\frac{4.0}{30} \frac{5.3}{23} \frac{4.5}{7}$

$\frac{4.1}{0} \frac{4.7}{6} \frac{8.2}{19} \frac{10.2}{23 \text{ creek}}$

✓  
 1049.12 ✓  
 6.09 1051.56 3.65 1045.47  
 139 6.4 1045.2  
 " "  
 140 4.6 1047.0  
 141 5.3 1046.3  
 141+39 5.0 1046.6  
 142 4.8 1046.8  
 142+59.4 4.3 1047.3  
 145+60 2.0 1049.6

$\frac{7.4}{30}$   $\frac{6.5}{11}$   $\frac{6.5}{8}$   $\frac{6.4}{0}$   $\frac{6.9}{6}$   $\frac{8.7}{10}$   $\frac{8.3}{25}$   $\frac{9.0}{75}$  Creek 80

$\frac{2.6}{30}$   $\frac{4.6}{0}$   $\frac{4.5}{5}$   $\frac{10.8}{15-24}$   $\frac{8.8}{30}$   $\frac{8.0}{40}$   
 Creek

$\frac{4.0}{30}$   $\frac{4.6}{25}$   $\frac{5.9}{18}$   $\frac{5.1}{13}$   $\frac{5.3}{0}$   $\frac{4.6}{5}$   $\frac{5.9}{10}$   $\frac{10.8}{29-40}$   
 $\frac{1042.9}{8.7}$   $\frac{1045.4}{6.2-3.7}$   $\frac{1047.8}{11.8}$   $\frac{1046.6}{5.0}$   $\frac{1047.6}{4.0}$   $\frac{1045.8}{11.8}$   $\frac{1042.6}{9.0}$   $\frac{1041.6}{10.0}$   
 Creek  
 40  
 Creek

$\frac{5.7}{30-15}$   $\frac{5.0}{8}$   $\frac{4.8}{9}$   $\frac{5.3}{14}$   $\frac{6.2}{14}$   $\frac{6.5}{30}$

$\frac{5.2}{25}$   $\frac{4.7}{16}$   $\frac{5.5}{14}$   $\frac{4.5}{11}$   $\frac{4.3}{0}$   $\frac{4.7}{9}$   $\frac{5.8}{16}$   $\frac{4.2}{25}$

## Pipe Required for Township Culverts

Station	Pipe	
	12"	15"
5+78	32'	
15+61		36
19+48.3	12	
24+97.5	16	
38+96.5	32	
42+96.5	32	
46+91		32
52+98		36
55+89.5		12
63+16 West		36
63+16 East		12
79+76		40
92+53		32
100+00	36	
105+24		12
117+00		-32
Total	160	280

9.29.42  
Pomeroy  
Gundersen

DINES CORNERS  
ROAD T.H. 144

11 to

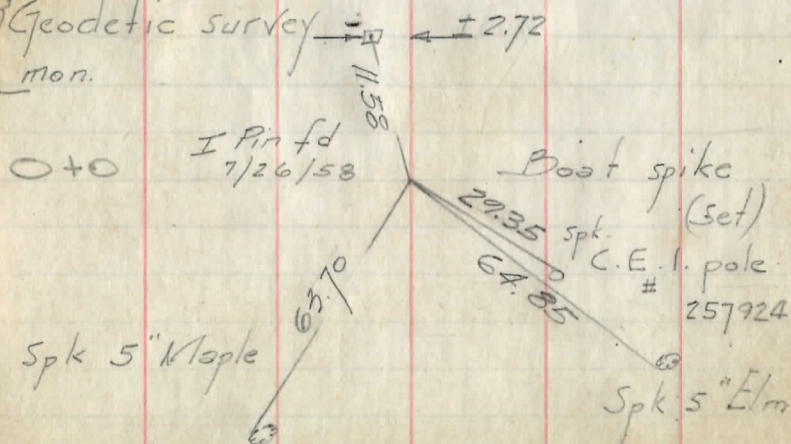
8 to 6.20

A = 0° 50' Lt

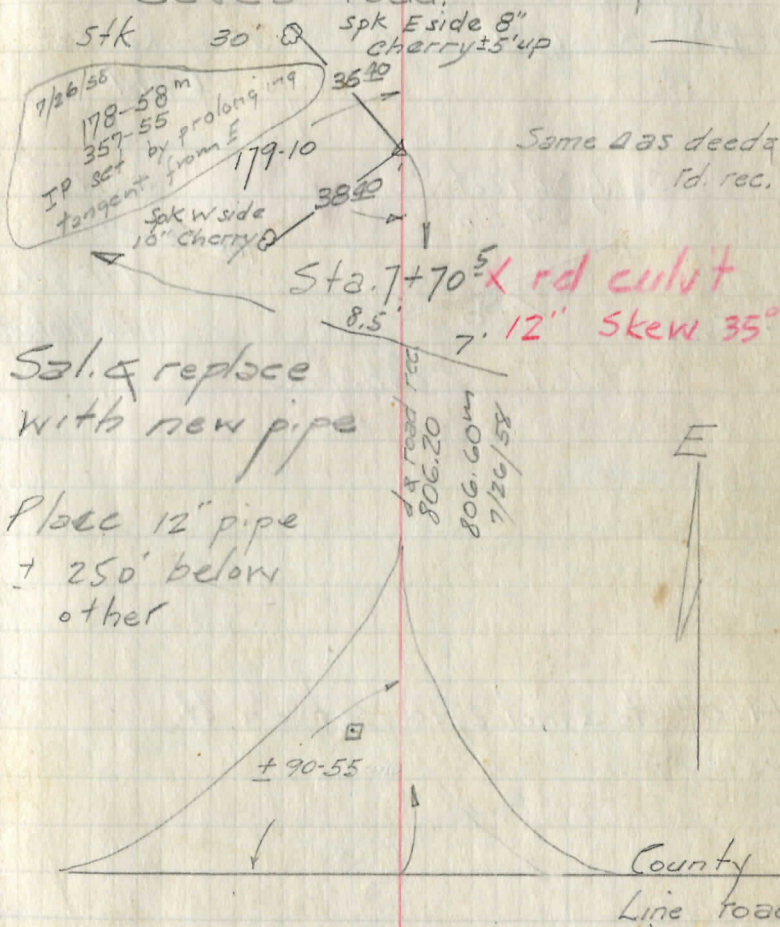
△ Boat spike set

Note: See County Line Rd. Survey  
(Fd. Bk. # 166 pg. 30) for additional  
information re: intersection

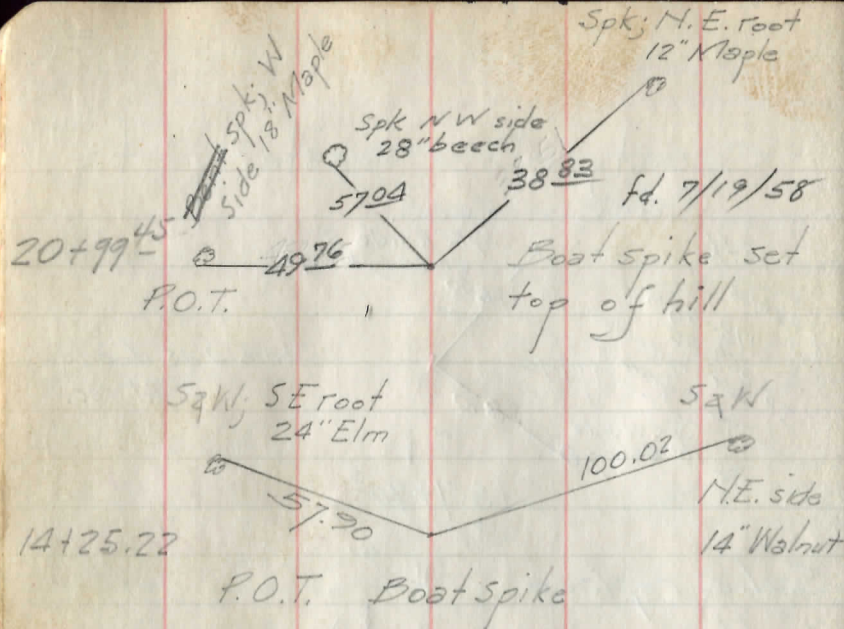
Clatsop Regional Survey  
Geodetic survey  
mon.



County line easterly to  
Caves Road



Note: Stakes set every odd Sta.  
at 30' Rt unless otherwise noted

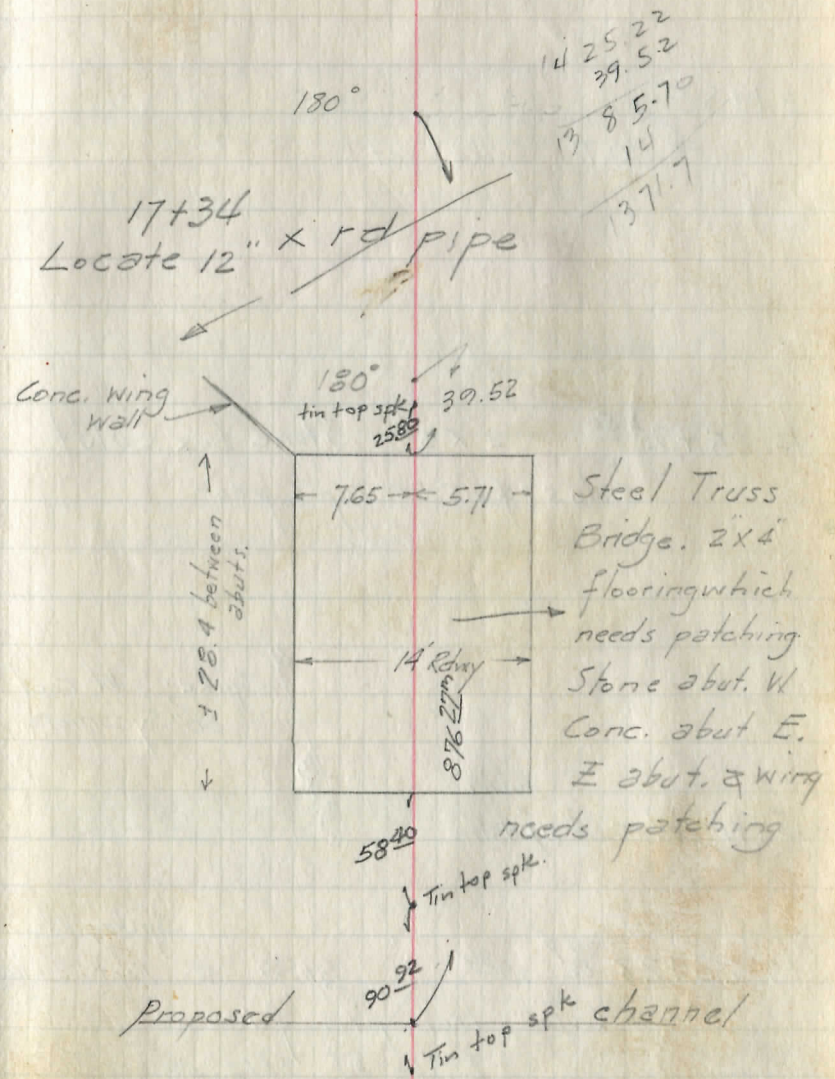


14+0 to incl. 27+0 set on Lt.

13+85.70

spike

876.27



31+857

P.O.T. Spike set

Sta. 25+95<sup>50</sup> 2'x3' Stone box cul't  
sides = fair top = poor

twin  
S&W; W. root 11" Ash

Sta. 23+28<sup>297</sup> @ 29<sup>36</sup>

P.O.T.

Iron pin fd  
I Pipe fd 7/19/58

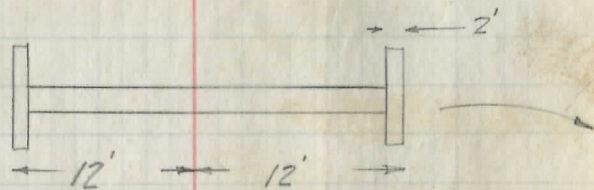
Spike; S.W. root  
30" Sycamore.

Spike; W.  
root 22" Elm

46<sup>87</sup>

spt S side  
20" MAPK

180°



Cherodan Corp.

Cherodan Corp.

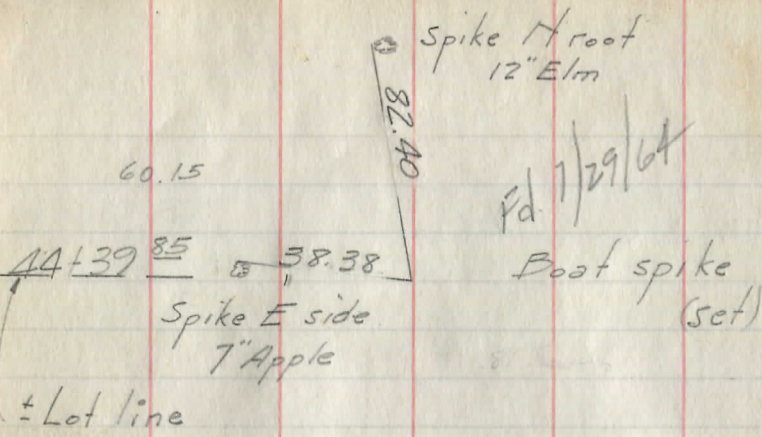
P.L.

180°

P.L.

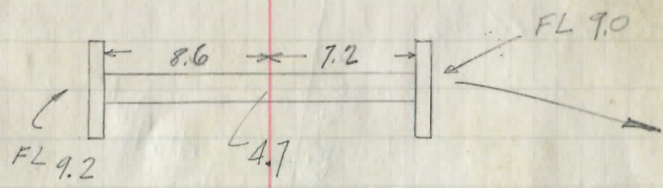
Bishop

Ginn

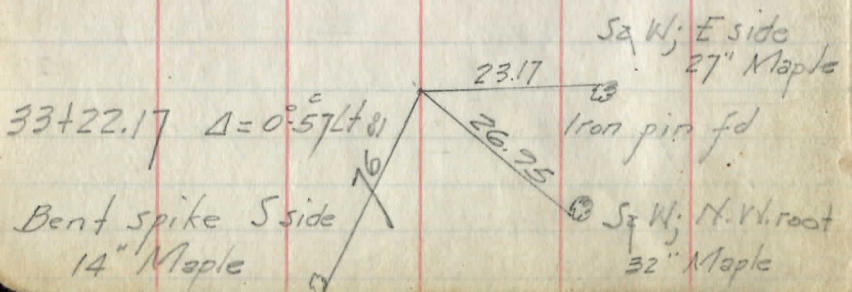


179-34-30  
359-09

37+18.5 3'x3' Stone Culvert.  
Very poor



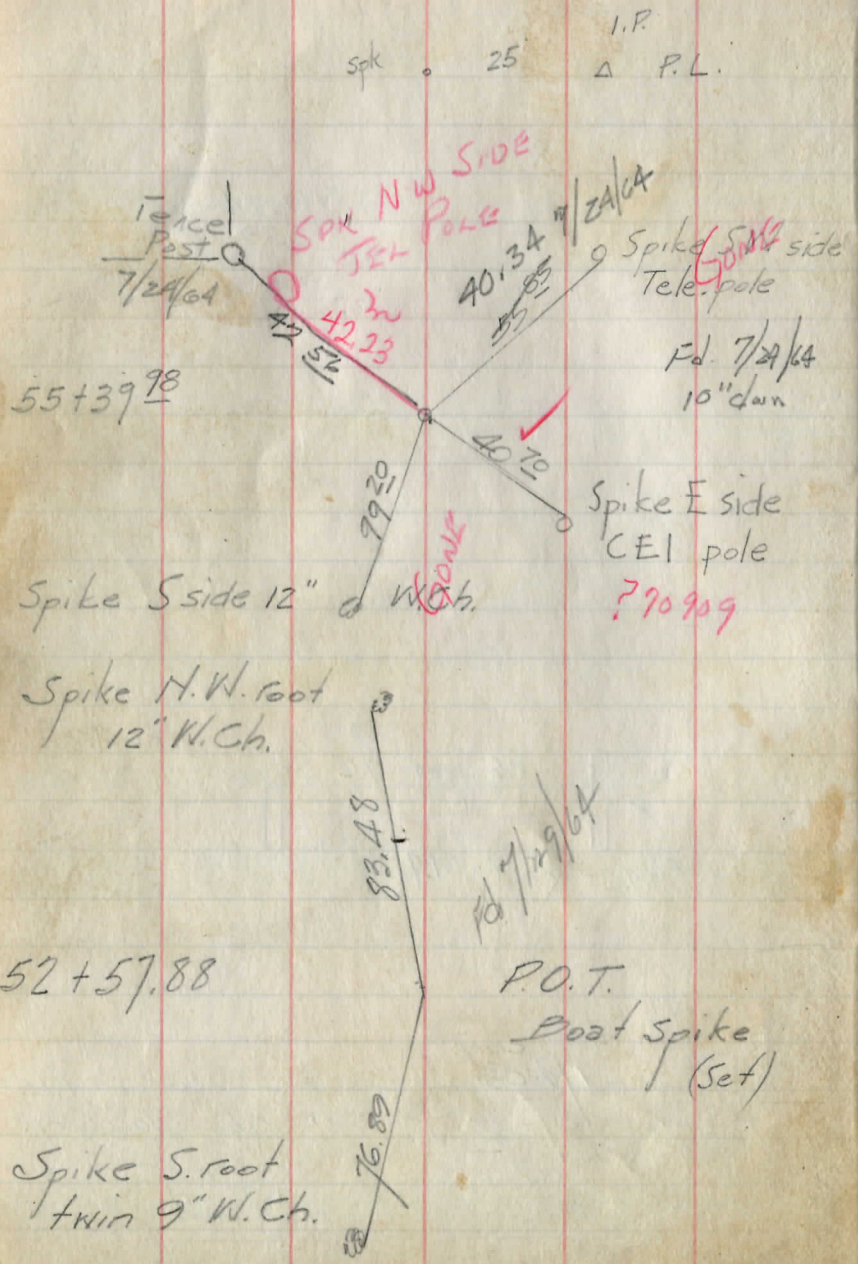
Scanlon



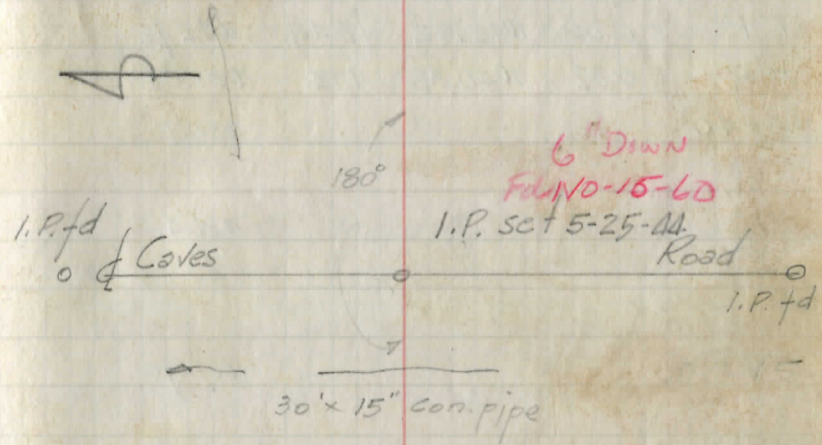
Comp.  
179-03

P.L.  
Cherodan Corp.



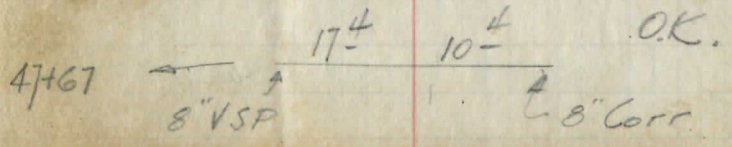


Notes: No intersection made.



Tree Rem  
||||

Channel ch  
110' Av cut 2.5'  
113 8" VSP 51+15  
brush logs



5-27-43

Pom  
Snyder  
Hall

+

H.I.

-

=

B.M. 1.74 1055.20 1053.46

T.P. 0.20 1042.92 12.48 1042.72

T.P. 9.32 1040.38 11.86 1031.06

55+40 1030.7

55 1031.4

54 1033.90

53 1036.1

52+60 1037.2

52 1035.4

51 1034.9

T.P. 4.17 1039.02 5.53 1034.85

50 1035.4

49 1033.7

## DINES CORNERS

29

S & W; SW root 26" Buckeye ± 300' S  
on Caves Rd West side road ± 20'

H E S

9.70

7.8 6.7 8.5 9.8 9.0 9.0 9.2 9.9 7.6 6.5 5.5  
30 18 10 8 6 9 11 15 18 30  
127.8 6.4 6.5 7.6 6.7 6.5 - 7.1 1.3 1.0  
30 19 12.9 7 6 9 17 306.3 4.4 5.1 4.5 4.3 4.5 5.5 2.0 1.3  
30 11 8 7 .7 9 16 30

3.2

8.3 5.8 5.0 - 5.8 4.2 0.2  
30 15 7 9 13 25  
20 1611.3 10.3 5.7 5.5 5.9 7.1 6.3 5.6 2.0  
30 23 9 9 11 14 16 30  
196.5 4.5 3.6 3.7 4.7 3.2 1.7 +0.3  
30 19 8 10 12 18 305.8 4.7 5.7 5.3 6.3 5.6 5.3 5.5 7.0 2.8 1.3  
30 21 15 12 8 6 9 11 17 30

1139.02

48

1030.80

47

1030.4

46

1027.9

T.P.

0.37

1027.74

11.65

1027.37

45

1026.2

44

1021.34

43

1013.6

T.P.

0.19

1015.42

12.51

1015.23

42

1009.7

6-9-43 Pom Hall Boone

B.M.

0.97

1009.76

6.63

1008.79

41

1007.1

H

5

30

this Sta only

5.2	7.0	9.3	8.0	8.2	8.7	9.6	11.0	11.5
26	16	11	8		13	19	24	30
30								

10.5	8.8	8.6	8.3	8.9	5.6	4.6
30	14		11	12	18	30

10.1	11.4	11.1	11.2	11.9	9.4	8.9
20	9		10	12	17	30
30						

3.9	1.8	2.6	2.0	1.5	1.4	2.8	1.1	40.7
30	9	8	7		10	14	21	30

4.5	3.5	6.5	6.4	-	6.9	6.2	0.6	
30	24	9			6	10	12	21
								30

12.6	14.3	14.1	14.3	15.3	12.7	9.7	4.3
23	19		7	10	14	18	30
30						20	

7.1	6.8	6.0	5.7	6.4	4.6	0.3	13.5
30	17	12		9	20	27	37

Spike S. root 36" Elm 41 ± 50 20 North

1.1	2.4	2.7	2.4	2.7	2.6	3.3	2.8	3.1
30	13	10	8		6	9	14	30

40 1005.6

39 1005.1

38 1004.5

Culvt gone to H-1

37 1004.5

36 1004.4

T.P. 8.41 1102.88 5.29 1004.47

35 1005.7

34 1008.6 ✓

T.P. 6.60 1109.11 0.37 1012.51

33 1012.0

32+50 1014.7

1.9	5.1	5.7	5.4	4.5	4.2	4.1	4.4	4.5
28	22	18	14	11	8	18	30	
35								

5.5	5.3	6.1	6.9	5.3	4.8	4.7	4.7	5.4	5.6	6.2	4.5	4.9	5.2
35	24	21	18	13	8	5	8	15	17	20	23	30	

6.2	6.3	7.9	5.9	5.2	5.3	5.5	7.3	5.8	5.3
35	24	18	12	6	£	14	17	19	30

9.3  
30

6.6	6.4	7.6	5.4	5.3	5.4	6.1	7.6	7.0	6.8
35	28	17	7	7	9	14	17	30	

6.4	6.8	6.6	-	5.4	5.5	6.8	7.3	7.5
30	19	11	6	6	9	18	30	

3.9	7.6	8.5	7.7	7.1	7.2	7.3	8.0	7.4	4.8	5.4
20	12	10	8	7	6	9	11	18	30	
30										

3.0	2.7	2.8	5.2	4.4	4.3	4.4	5.3	3.2	3.5	3.7	3.8
30	18	11	7	6	8	10	14	17	21	30	

5.9	5.7	7.6	7.0	7.1	7.0	7.6	5.5	4.6
30	14	10	9	3	6	9	30	

4.4

31485

1013.8

31

1007.6

T.P. 4.05

1100.22 12.94

1006.17

30

996.0

T.P. 0.24

1106.41

1006.17

T.P. 0.46

1109.97 12.90

993.51

29

986.4

28

982.9

T.P. 1.68

1108.59 11.06

982.91

27

981.0

1109.11

H E

S

32

41 39 5.5 5.3  
30 21 11

5.3 5.8 4.1 4.0  
5 6 10 30

7.5 7.4 7.8 11.6 11.7 11.5  
30 21 14 9 6

11.6 12.1 7.7 7.6  
5 7 15 30

6.0 5.1 - 14.2  
30 20 6

14.0 13.8 8.8  
7 11 30

29+25 Beg. cut sect N side

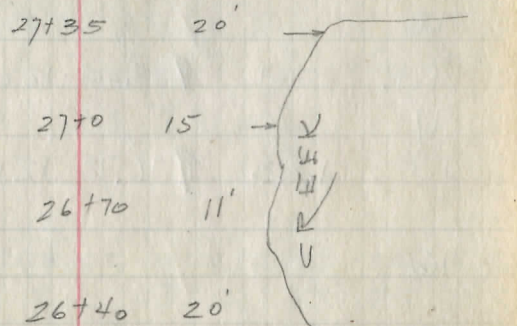
- - 7.6  
30 9

7.7 9.4 9.7  
13 18 30

11.0 11.3 12.0 - 11.1  
22 10 7 4  
30

11.1 12.2 12.2  
8 12 30

4.6 4.2 4.7 3.8 3.6 4.1 5.4 6.9 5.1 4.9 + 0.1  
30 17 13 10 4 10 15 20 30 40  
CK



colut dined pool

26 779.7  
 25 779.3  
 24 782.1  
 B.M. 5.26 778.63  
 T.P. 12.30 795.08 2.31 782.28  
 23 790.1  
 T.P. 13.12 1001.75 0.45 794.63  
 22 1000.0  
 21 1004.6  
 20 1000.3  
 T.P. 1.18 799.95 8.98 798.77  
 19 793.3  
 18 788.4  
 T.P. 0.27 788.20 12.02 787.93  
 17 1080.4  
 T.P. 1.23 776.78 12.65 775.55 Stone  
 16 768.3  
 T.P. 0.29 767.75 9.32 767.46

4.9  
 6.1 6.1 5.4 5.3 5.4 6.9 7.3 8.3  
 30 12 6 5 5 17 30  
 2.8 3.3 2.7 2.5 2.6 5.6  
 30 10 7 16 30  
 Spk N side twin Bycomore 26+15  
 25 Rt. (18 E of Colot)  
 +1.3 0.0 6.2 5.3 5.0 4.7 2.2 3.4  
 30 20 8 6 13 20 30  
 3.0 4.1 8.8 7.9 7.8 7.7 8.7 6.6 6.2 7.3  
 30 14 8 5 6 8 10 18 30  
 2.8 2.8 3.6 3.2 3.8 3.0 3.4  
 30 15 9 £ 8 16 30  
 4.7 5.1 8.5 7.5 7.6 8.2 5.8 5.3 6.2  
 30 13 8 5 7 11 20 30  
 3.1 3.4 7.1 6.8 6.7 6.6 7.6 4.0 3.5 3.8  
 30 15 9 7 4 7 11 18 30  
 10.1 9.8 10.7 12.4 11.6 11.6 - 12.5 9.9 8.8  
 30 17 10 8 5 £ 6 8 12 30  
 8.4 8.2 2.3 8.1 7.8 7.9 0.6  
 30 26 12 6 11 18 30  
 7.9 8.9 8.0 7.4 7.5 9.4 8.5 - 4.3 +3.9 +4.2  
 25 22 20 15 11 7 7 12 21 30  
 30

767.75 ✓

15

761.8

14

759.5

T.P. 6.89  
ctr brge

765.18 ✓

9.46

758.29 ✓

13

5.76

759.4

758.9

12+50?

± 12' to top ck bk.

12

760.6

B.M.

3.96

761.22

T.P. 10.88

775.65 ✓

0.41

764.77

11+10

ch fill to cut South

11

766.8

10+70

= Max. cut So.

T.P. 10.89

786.28 ✓

0.26

775.39 ✓

10

776.8

9

785.7 ✓

T.P. 10.92

796.98 ✓

0.22

786.06

9

H

☒

5

34

8.0 7.0 6.7 7.8 6.5 5.9 6.0 6.2 6.7 5.9 6.2 6.4  
30 24 17 15 11 5 4 3 4 7 11 17  
30

9.9 9.8 9.4 9.0 - 8.3 - 8.8 9.3 9.8 10.0  
30 25 18 11 8 6 9 14 22 30

± 3' bank 12.5 7.3 6.8 6.4 6.3  
on out 20 16 13 9  
ck 37

6.6 6.7 7.0 7.7  
8 10 15 30

± 11.8 5.8 5.3 4.8 4.7 4.4 4.6 4.3 4.7 5.1 5.4  
36 30 26 18 12 9 5 8 13 20  
ck 30

Spk Sroot 20" Elm 12+00 25' Lt (on  
bk of ck.

7.2 6.7 7.6 7.2 9.2 8.9 7.5 7.1 4.4 3.5  
28 22 18 14 11 4 8 11 16  
30 30

± 24.0 12.5 9.4 7.7 7.1 9.5 9.0 9.7 7.1 +1.0 Level  
30 15 11 8 4 10 12 16 24

down  
down  
& down 10.6 6.9 +0.4 0.5 0.6 0.4 1.1  
26 18 6 4 8 9

1094.4  
2.6 level  
21

8  
T.P. 9.42 1006.23 0.17 9793.0  
9796.81

2.2 0.2 4.2 3.9 4.0 - 4.5 2.0 +1.0 +1.3  
30 15 9 7 3 4 6 10 30

7  
977.7

9.3 9.7 8.7 8.0 8.4 8.3 8.5 - 6.4 5.8 6.0 5.9  
30 26 20 16 12 10 5 8 13 19 30

6  
1000.5

6.6 6.3 5.9 5.6 5.7 6.3 4.7 3.6 3.7 3.3  
30 24 11 9 4 8 14 20 30  
18

5  
T.P. 10.04 1013.93 2.34 1003.5  
1003.89

2.1 1.9 1.4 3.4 2.4 2.7 3.0 10.8 +1.0  
30 22 15 11 8 5 10 30

4  
1007.0

5.1 7.4 6.8 6.9 6.7 7.0 6.0 6.2 6.9  
14 10 8 4 6 10 16 30  
30

3  
T.P. 8.72 1022.74 0.91 1010.1  
1013.02

3.4 3.5 4.5 3.9 3.8 3.9 4.3 3.4 3.5  
30 13 9 7 4 7 11 30

2  
1012.7

7.6 9.4 7.0 9.6 7.8 7.6  
14 9 6 10 18  
30 30

1  
1016.8

4.1 5.7 5.0 4.9 5.0 5.4 4.2 4.0  
13 10 8 6 7 12 30  
30

0  
B.M. 6.6 115.1  
6.29 1015.45

Cleve. Regional Survey Monument  
See pg 24 for Loc. <sup>Marked</sup> 857

RE X SECTION OF SOME  
STA. DINES 43

BM. 6.51 1015.30 1008.79

42 1009.6

43 1013.6

T.P. 12.83 1027.92 0.21 1015.09

43

44 1021.32

45 1026.2

T.P. 8.14 1035.62 0.44 1027.48

46 1027.8

47 1030.4

inlet F.L. 7.2 1028.4

48 1030.92

11

5

36

5-29-44  
Pom-Jackson-  
Myers

6.8 6.2 5.6 5.7 5.9 6.2 4.5 0.2 up  
19.5 14.5 6.5 4.5 9 20.5 26.5  
30

14 0.0 1.4 2.0 1.7 2.4 3.2  
30 21 18 7.5 6.5 8.5  
12.5

1024.4  
3.5  
30

4.5 3.7 5.9 6.6 6.6 6.7 7.1 5.1 0.9  
30 24 13.5 8 5 11 17 22.5  
30

4.0 2.6 1.7 1.4 2.8 10.5  
30 7.5 8 13.5 25  
16.5 30

7.4 7.2 8.0 7.8 7.7 8.6 5.9 6.1  
30 15.5 8.5 7.5 13 20.5 29

6.9 6.2 4.9 5.4 5.2 5.1 4.9 5.4 2.0 1.3  
30 22 15.5 7 8.5 10.5 11 17.5 30

8.1 7.0 5.5 5.2 4.7 - 5.9 4.7 3.4 1.5  
30 21 14 7.5 8 10 13 18 28

B.M. 5.82 984.45 978.63

25 5.1

24

T.P. 12.70 996.90 0.25 984.20

23 989.9

Note: New cut 22+20 to 23+60

B.M. 6.51 985.14 978.63

8.61 991.57 2.18 982.96

29 986.0

T.P. 13.22 1004.69 0.10 991.47

30 996.0

New cut on S 29+85 to 30+67

2.6 3.0 2.5 2.3 2.2 2.4 15.4

25 15.5 6 8 16 28

30 22

0.7 2.9 6.8 7.9 7.1 7.0 6.9 6.5 3.7 4.6

30 18 10.5 8 6.5 5.5 13 18 24

4.8 5.2 5.3 5.6 5.4 6.1 7.3 7.5

22.5 14.5 6 7.5 14 21.5 30

+1.9 6.2 8.6 8.7 8.5 6.7 2.1

22 12 6.5 8.5 19 28.5

Young Adams  
Donor

X-500 Russell Twp. 8-61  
78° SUNNY CAVES Rd.

	+	HI.	-	Elev.	
Bm #1	2.17	102.17		100	use
Bm #2	1.82	96.82	6.69	95.48	
			2.78	94.04	use
			11.66	85.16	
Bm #3	1.44	86.60	8.67	77.93	
	5.53	83.46	6.71	<del>77.75</del>	use
	11.61	72.70	2.17	81.29	
Bm #2	8.09	100.33	.66	92.21	
			6.33	94.00	
			.65	99.68	
Bm #1	5.29	104.97			
			5.01	99.96	
Bm #3	0.72	78.17		77.75	
Bm #4	1.55	68.80	11.22	67.05	
			10.20	58.80	use
	3.11	61.54		58.80 <sup>em.</sup>	
Bm #5	3.89	57.05	8.35	53.16	
			8.52	48.53	use
	9.37	62.33	4.11	52.91	
			3.92	58.81	
	10.81	69.74	3.00	59.33	
	10.85	79.63	0.56	69.18	
			1.85	74.78	
Bm #5	1.12	52.65		48.53	

sta 0+9  
CET of CAVES S. side # sk. 87 (spt. N side)  
# 53176  
CET sta 11425 spt W. side

CET # 53171 sta 11470 spt. W. side

73.26  
6.71  
76.5

CET # 53565 sta 31480 spt. E. side

CET # 602580 sta 50160 last CET. on W. side  
spt E. side

52.65

	+	HI	-	Elev.
BM#6	2.46	45.11	10.00	42.65
			9.77	<del>38.31</del>
BM#5	9.25	52.30	2.06	43.05
			3.75	<del>41.55</del>

BM#1 0+0	5.36	105.36		100
-------------	------	--------	--	-----

1+0

2+0

3+0

TP 4+0	14.6	99.71	7.11	98.25
-----------	------	-------	------	-------

4+0

5+0

6+0

TP 7+0	6.25	100.78	5.38	94.33
-----------	------	--------	------	-------

7+0

E. E W.

CEI# 170909 s/b. 62480 E. side spl.

99.9  
5.7

SR# 87

0.8	4.95	62	66	64	55	63	58	3.2	31		
30	20	17.6 17.7	16.3	15.3	14.3	10.9	15.5	21.5	30		
52	52	6.0	5.3			5.6	3.5		32		
30	19.2	18.3 16.2	11.2			10.8	20		30		
4.5	5.2	7.4	7.65	5.3	7.6	7.2	7.8	8.2	7.35	4.7	4.6
30	22.3	18	16.2	16.8 16.3	12		10.2	15.9	16.5	27.2	
4.0	4.95	5.1	5.25	5.2	4.9	4.6	5.2	5.5	5.7	4.5	4.0
30	18.8	17.6	16.3	16.2 11	16.5		12.8	16	16.5	23.5	30
5.3	5.9	6.65	5.8								
30	19.2	16	12.5								
6.5	7.1	7.3	6.1								
30	18.8	17.5 14.2	12.2								
5.2	5.8	6.6	7.2	6.8							
30	19.4	16.2	16.7 16.2	14.3							

	+	117 <sup>2</sup> 100.78 H.I.	-	Elev.	
810					
910					
1010					
1110					
Btm #2	0.23	94.27	6.75	94.03	OK
1210					
T.P.	4.91	87.66	11.52	82.75	
1310					
T.P.	3.93	79.83	11.76	75.90	
1410					
1510					
1610					
1710					
TR	6.06	79.97	5.92	73.91	
1810					
1910					
Btm #3			3.16	76.81 <sup>95</sup>	OK

	E					95.6	W.				
31	34	49	58	52	57.5	5.8	5.3				
30	23 <sup>3</sup>	16 <sup>6</sup>	15 <sup>0</sup>	12 <sup>2</sup>	92.9	15	30				
71	73	80.5	85	83	79	8.35	8.8	8.3	7.6	7.9	
30	19 <sup>2</sup>	16 <sup>0</sup>	14 <sup>5</sup>	13 <sup>0</sup>	82.5	11 <sup>2</sup>	15	15 <sup>5</sup>	18 <sup>2</sup>	30	
71	8.3	10.	9.2		91.9	9.5	10.0	9.9	10.	10.	
30	19 <sup>0</sup>	14 <sup>2</sup>	11 <sup>2</sup>		80.4	12	16	17 <sup>2</sup>	21 <sup>5</sup>	30	
8.1	8.3	12 <sup>3</sup>	10.9		86.0	11.1	12.2	11.0	10.3		
30	23 <sup>2</sup>	17	11 <sup>2</sup>		80.1	10.8	17 <sup>0</sup>	18 <sup>1</sup>	21	out	
32	3.6	8.5	10.1	9.0	8.3	7.8	9.0	7.7	5.9	5.9	
30	27 <sup>2</sup>	17	16 <sup>0</sup>	12	75.4	11	16 <sup>3</sup>	17 <sup>5</sup>	21	24	
			10 <sup>5</sup>		76	8.3	9.3	7.6	5.1	5.5	
1.2	1.65	9.9	8.6		73.5	10.6	15 <sup>3</sup>	17 <sup>6</sup>	21.6	30	
30	27 <sup>0</sup>	12 <sup>3</sup>	12 <sup>0</sup>		72.7	17 <sup>2</sup>	17 <sup>6</sup>	21.6	30		
0.4	1.0	0.7	5.7	0.1	71.4	0.7	derive		4.3		
30	21.8	10 <sup>5</sup>	12 <sup>5</sup>	10 <sup>3</sup>	73.5	14			30		
5.5	6.6	7.6	6.6		6.3	7.0	8.0	7.4	7.9	8.3	
30	16 <sup>0</sup>	10 <sup>2</sup>	11		72.7	10 <sup>0</sup>	16 <sup>2</sup>	17 <sup>0</sup>	19	25	30
7.8	8.3	8.7	7.0		71	7.9	8.8	8.4	8.9	9.4	
30	17 <sup>6</sup>	16 <sup>3</sup>	11.2		73.4	17	18 <sup>0</sup>	22 <sup>2</sup>	30		
32	4.0	7.0	7.6	6.9	71	7.0	7.9	5.4	6.2		
30	22	14 <sup>3</sup>	13 <sup>2</sup>	11 <sup>2</sup>	75.1	15	17 <sup>2</sup>	21 <sup>5</sup>	30		
1.8	2.1	5.9	5.2		4.85	5.5	5.1	derive	5.6		
30	22	14	10 <sup>0</sup>		74.5	16 <sup>3</sup>	17 <sup>5</sup>				
4.6	4.9	6.1	6.7	6.6	5.5	6.4	7.1	6.5	6.1	6.0	
30	22	17	15	10 <sup>3</sup>	11	15 <sup>2</sup>	17 <sup>0</sup>	25	30		

76.75

	+	H.I.	-	Elev.
BTH#3	1.0	77.75		76.75
2040				

2140

2240

T.P.	1.46	71.30	10.91	66.81
2340				

2440

2540

2640

	1.63	61.91	10.99	60.31
2740				

2740

2840

	2.36	52.35	11.95	49.99
2940				

2940

3040

41

	E	W
2.0	2.9	3.6
30	21	15.8
37	49	2.7
43	122	5.1
23		55
152		30

3.3	50	4.3	40	4.1	drive	3.6
30	152	112		122		30

5.5	72	9.1	8.6	8.1	8.2	9.1	8.2	5.9	6.2
30	182	162	132		12	152	162	222	30

4.1	52	6.5	5.6	5.3	5.6	6.3	5.6	2.5	2.3
30	162	132	102		122	142	152	222	30

7.7	80	8.6	8.0	7.6	8.2	8.8	8.2	8.0	
30	162	122	122		122	142	152	30	

9.1	95	11.1	9.1	8.7	9.3	11.3		11.1	
30	20	182	14	102		112	17	30	

7.7	8.4	8.8	8.7	9.0	8.6	8.9			
30	15	112		182	192	30			

0.1	1.0	3.2	3.9	4.5	4.1	3.9	4.3	5.2	1.1	1.6
30	212	182	16	152	118		12	152	21	30

7.0	7.5	8.9	10.1	9.3	9.2	9.1	9.7	10.4	7.7	7.8
30	222	182	162	152	132		122	152	192	30

0.7	1.8	2.5	3.1	3.1	3.1	3.1	3.1	3.6	3.0	3.7
30	212	162	11				82	102	152	182

3.4	4.6	6.0	6.2	6.8	6.2	4.6	6.3	6.8	6.2	4.5	4.5
30	28	172	162	152	132	55	112	132	142	192	30

52.35

52.35

3110  
3210  
3310

10.83 61.93 12.5 51.10  
BM# 4.52 57.21 OK

3410  
3510  
3610  
3710  
3810

4.56 57.79 8.76 53.23

3910  
4010  
4110  
4210

E E W

71	75	8.0	73	46.4	76	8.7	8.2	88.92
30	16 <sup>2</sup>	15	12	70	11 <sup>2</sup>	12 <sup>2</sup>	16 <sup>2</sup>	28 30
88	8.2	10.0	68	45.9	6.5	6.9	8.6	10.2 83 93 10.
30	21 <sup>2</sup>	11	11 <sup>2</sup>	8 <sup>2</sup>	14 <sup>2</sup>	15 <sup>2</sup>	17 <sup>2</sup>	22 <sup>2</sup> 30
40	43	4.9	44	48.2	4.15	4.9	5.7	4.5 50
30	19 <sup>2</sup>	16 <sup>2</sup>	11 <sup>2</sup>	11 <sup>2</sup>	14 <sup>2</sup>	15 <sup>2</sup>		30
45	5.5	9.0	8.5	53.6	8.3	8.8	9.7	8.5 53 52.5
30	19 <sup>2</sup>	16 <sup>2</sup>	11 <sup>2</sup>	11 <sup>2</sup>	14 <sup>2</sup>	15 <sup>2</sup>	21 <sup>2</sup>	30
27	3.6	5.3	5.9	56.7	5.7	5.8	6.4	6.1 6.5
30	20	16 <sup>2</sup>	15 <sup>2</sup>	12	13 <sup>2</sup>	15 <sup>2</sup>	19 <sup>2</sup>	30
49	5.6	6.7	5.7	56.4	5.5	6.3	6.8	6.5 6.8
30	18 <sup>2</sup>	15 <sup>2</sup>	9 <sup>2</sup>	13 <sup>2</sup>	15 <sup>2</sup>	18 <sup>2</sup>		30
50	5.7	7.9	7.0	58.4	6.5	6.7	live	5.2
30	19 <sup>2</sup>	15 <sup>2</sup>	11 <sup>2</sup>	12 <sup>2</sup>				30
90	8.9	9.7	9.0	53.5	8.4	9.3	9.8	8.6 7.2 6.6
30	17 <sup>2</sup>	15 <sup>2</sup>	12 <sup>2</sup>	16	16 <sup>2</sup>	17 <sup>2</sup>	21 <sup>2</sup>	30
51	5.8	7.3	5.5	52.7	5.1	5.9	7.1	7.1
30	20 <sup>2</sup>	16 <sup>2</sup>	11 <sup>2</sup>	12	16 <sup>2</sup>			30
3.8	4.7	5.2	6.1	52.8	5.4	5.6	6.5	5.9 6.3
30	18	16 <sup>1</sup>	15 <sup>2</sup>	11 <sup>2</sup>	10 <sup>2</sup>	16 <sup>2</sup>	17	30
40	8.8	6.8	5.5	52.3	5.5	6.2	6.7	5.5 14 4.6
30	19 <sup>2</sup>	15 <sup>2</sup>	12 <sup>1</sup>	13 <sup>2</sup>	16	16 <sup>2</sup>	20 <sup>2</sup>	30
7.2	8.0	8.9	8.4	50.0	7.8	8.3	9.1	8.0 7.6 7.9
30	17 <sup>2</sup>	15 <sup>2</sup>	13 <sup>2</sup>	10 <sup>2</sup>	13 <sup>2</sup>	18 <sup>2</sup>	20 <sup>2</sup>	30

57.79

57.79

4310

4340

thron apple drive

440

445 52.76 9.08 08.31

4540

4640

4740

4840

4940

5040

Bm<sup>45</sup>

1.41 48.94 5.18 47.55 47.53

5140

5240

5340

43

E

L

W

8.8	8.4				49.7	8.7	9.3		9.5
30	16				81	13	15.5		30

						7.3			6.6
						100'			150'

6.8	7.6	8.1	8.1	7.5	50.8	7.4	7.7	5.1	4.2
30	18.4	17.5	16.4	13.4	50.1	13	15	19.2	30

2.2	2.7	3.2	3.7	3.4	30.7	3.2	3.4	3.5	0.1	4.0	4.6
30	21	18.2	16.4	15	12	9.5	11.4	13.5	15.4	16.2	25.30

6.5	7.0	7.5	7.5	8.1	7.3	6.7	7.3	7.6	5.7	5.3
30	19.5	18	16.1	15.2	12.2		13.2	15.2	19.6	30

9.2	9.2	9.4	8.1		45.1	7.7	8.7	9.2	10.6	10.5	8.9	9.4
30	16	15	10.5		7.7	10	17.2	18.2	20.2	22	30	

5.4	7.2	7.8	7.2		46.3	6.5	6.8	7.2	7.6	7.2	6.8
30	15	12.3	10		6.5	9.2	14.4	16.2	17.5	30	

4.4	5.2	5.4	5.2		48.0	4.8	5.3	6.0	5.0	0.7
30	14.9	14.2	11.5		4.8	10.5	15.2	19.5	30	

9.5	7.6	8.0	7.4		46.1	6.7	7.1	drive	6.0
30	14.5	13.1	11.1		6.7	13			30

2.7	3.5	6.3	5.8	5.0	48.7	2	5.6	6.4	6.5	5.3	5.3
30	17.8	13.2	10.2		5.0	11.9	15.4	16.2	18.4	30	

5.7	6.4	7.3	7.8	7.2	42.0	6.9		7.3	Drive	7.5
30	12.4	13.2	12.6	6.4	6.9	17.9				30

7.2	8.1	9.4	7.8	7.5	41.4	7.5	8.4	kawa	9.7
30	16.2	13.1	10.2		7.5	14.9			30

	+	48.94 HI	-	Elev
54+0				
TP	8.76	54.31	3.39	45.55
55+0				
56+0				
57+0				
58+0				
TP	0.68	50.46	4.53	49.78
60+0				
61+0				
TP	2.91	47.57	11.78	38.68
BM#6			7.29	34.30 34.34
62+0				
63+0				

See Field Book 310 page 6  
X-sec. Dives To Fairmount

	E	R	W
2.6	3.6	5.4	6.4 5.7 5.3
30	18 <sup>2</sup>	14 <sup>2</sup>	12 <sup>2</sup> 13 <sup>1</sup> 7 <sup>2</sup>
6.0	6.7	8.6	9.4 9.2 8.0
30	21 <sup>9</sup>	14 <sup>3</sup>	13 <sup>7</sup> 11 <sup>2</sup>
10.8	12.4	12.7	10.4 10.0
30	21 <sup>5</sup>	14 <sup>8</sup>	11 <sup>2</sup>
7.2	Lawn	8.5	8.4
30		12 <sup>9</sup>	
1.2	1.5	5.1	5.9 5.3 4.9
30	23 <sup>2</sup>	15 <sup>8</sup>	15 <sup>2</sup> 11 <sup>2</sup>
1.8	2.1	4.7	4.1 3.7
30	20 <sup>8</sup>	15 <sup>2</sup>	11 <sup>2</sup>
1.7	2.7	5.8	6.0 5.9 5.3 4.1
30	19 <sup>2</sup>	15 <sup>3</sup>	14 <sup>7</sup> 13 <sup>2</sup> 12 <sup>4</sup>
8.1	9.4	12.8	12.5 11.9 11.1
30	20 <sup>8</sup>	15 <sup>2</sup>	13 <sup>9</sup> 11 <sup>4</sup>
6.6	7.4	8.9	9.2 8.6 7.9
30	20 <sup>2</sup>	17	15 12 <sup>5</sup>
11.8	11.8	14.8	12.1 11.2
30	22	20	17

43.6

45.3

44.3

45.9

49.4

50.6

46.4

39.4

33.7

30.4

Top  
Caves  
8-10-61

E. E. W.

0+0 5.6. #87  
 +30 25' between - 4" x 10"  
 +45 23' free row osage or  
 +70 22' 10' x 20' ash  
 +63 22' CEI  
 +63 map 13' x 28'  
 1+02 map 16" x 28'  
 +9 conc. side walk 15'  
 +38 maple 13' x 28'  
 light post 21'  
 +60 12' x 16' drive boilers 16'  
 +71 map 16" x 27'  
 +80 25' x ash 13"  
 +89 25' x elm 10"  
 2+00 5' apart - 7 pine pine row A 20'  
 +05 27' x ash 10"  
 27' triple x 25" ash  
 15' 16' x 12" conc.  
 +26 27' x quad ash 26"  
 +46 CEI 29'  
 +77 29' CEI  
 3+58 16' 12' x 16' corr  
 4+0 27' tree row osage  
 +13 29' CEI

E. E. W.

+10 30' x ash 10  
 +05 30' CEI  
 10+03 27' x osage 12"  
 +74 16' 20' x 10" corr  
 +39 CEI 29'  
 9+23 27' x elm 25"  
 +95 27' x osage 12"  
 +80 27' x triple map. 15"  
 +56 29' CEI  
 +53 27' x osage tree row beg.  
 +38 27' x osage 10"  
 +19 27' x 12" elm  
 9+10 16' 16' x 10" corr  
 +97 28' x 30" twin cherry x osage  
 7+60 CEI 29'  
 +83 28' end tree row (down)  
 +70 16' x 12" corr paved 16' 25' x elm 13"  
 6+06 26' drive no pipe  
 +89 CEI 29'  
 +44 16' x 12" corr paved 17'  
 5+0 27' x osage 12"  
 +86 28' x osage 10"  
 +27 27' x osage 12"  
 +14 29' CEI

E. & W.

+20 50' @ elm 12"  
 +34 16' 16' x 12" corr.  
 +56 28' @ elm 17"  
 +98 26' @ elm 13"  
 11+13 CEI 29'  
 +42 28' @ cherry 13"  
 +62 15' x 25' CONC. paved 15'   
 29'   
 12+86 16' 12" x 22'   
 corr.  
 +88 CEI 29'  
 13+03 29' 5" @ map 12"  
 +05 27' 5" CEI  
 +07 27' @ map 10"  
 +26 26' @ ash 15"  
 +41 27' @ map 12"  
 +51 27' @ map 10"  
 +71 27' @ ash 16"  
 +81 26' @ ash 12"  
 +95 17' 16' x 12" corr.  
 14+05 28' @ elm 10"  
 +06 29' @ twin 24" ash  
 +24 27' @ map 16"  
 +37 28' @ twin 10" cherry  
 +43 27' @ osage 13"  
 +63 CEI 29'

E. & W.

+95 28' tree row  
 +84 28' @ ash 10"  
 +80 28' @ cherry 13"  
 17+18 30' @ 16' dm  
 +80' 29' @ cherry 13"  
 +75" 30' @ ash 13"  
 +72 29' @ osage 12"  
 +51 18' 12" x 19" corr.  
 +40 28' @ 9422 6" elms  
 +36 CEI 29'  
 +17 28' 14" elm  
 +12 28' @ 13" elm  
 16+ ~~28' @ 14" elm~~  
 +87 28' @ 20" elm  
 186 CONC 10" x 20 17'  
 +60 15" CONC. 17' 21'  
 +55 21' @ ash 10"  
 +45 28' @ elm 18"  
 +37 27' @ ash 14"  
 +34 18' 15' vit. (cont of lawn)  
 +17 27' @ ash 14"  
 +16 28' @ ash 11"  
 15+03 27' @ ash 12"  
 +88 27' @ dm 12"  
 +75 27' @ ash 18"

	E.	W.
18+01	17'	12'x18'
+12	CEI 29'	
+13	30'	triple 8" ash
+66	28'	e/m 13"
+68	28'	osage 12"
+97	28'	cherry 12"
19+13	12'x20' CONC. 16'	
+22	28'	osage 12"
+21		pipe paved 12" corr. length?
+55	30'	B e/m 28"
+85	CEI #531181 29'	
20+15	28'	CEI
+16	29'	osage 12"
+9	29 1/2'	double ash 28"
+25	30	osage 15"
+58'	16'x12" corr 16'	
+81	29'	osage 12"
95	29'	osage 14"
21+01	16'	paved 20'x12" corr.
+13	12'x20' CONC. 16'	
+43	28'	ash 18"
+66	32'	ash 15"
+67	28'	"end tree row"

	E.	W.
+57	6" pine 23'	
+48	corr. 10'x21' 15'	
34+25	map. 15'	27 1/2'
+78	CEI (fence ends)	30'
33+0	fence 25'	
+12	19' 18'	18" CONC.
32+02	CEI 29'	
+90		28 1/2' CEI
+37		15' pine 18'x12" corr
31+10		26' end lawn plants
+31		26' (10) lawn plants
+30	CEI 29 1/2'	
30+0	fence start 30'	
+59	CEI 29'	
28+12	16'x12" 16'	
+98	CEI 29'	
26+01	No pipe	
25+15	CEI 29'	
24+96	1/2 20'	16 1/2' 14 1/2' CONC 15"
23+36	CEI 29'	
+25	12'x24 corr. 14 1/2'	
22+0	lawn vit pipe 8" 15'	

N E W.

+75 29' CEI

+84 15" map 23'

35+07 12" map 23'

36+44 28<sup>E</sup> CEI

+93 17' 18X12" corr.

38+11 28<sup>E</sup> CEI # 53356

+63 14'X12" corr 17'

39+74 28<sup>E</sup> CEI

+85 CEI 29<sup>E</sup>

38.95 16<sup>E</sup> 17<sup>E</sup> 15"X33" CONC.

40+91 15' long rail fence paved 29<sup>E</sup>

41+12 12"X12' 16'

+21 15' long rail fence 29<sup>E</sup>

+38 29' CEI

42+93 15' 17' 15" ? corr.

43+03 28<sup>E</sup> CEI

+15 CONC. 32'X15" 19' a THORN Apple De.

44+12 29<sup>E</sup> map 5"

+41 17' 12"X16' corr.

+67 28<sup>E</sup> CEI

45+7 16'X12" corr. 16'

+20 16'

46+23 16' 24'X12" 12"X24' corr.

E. W.

+82 Cast iron 19" 16' 16' 19" CONC. 19"

+46 CEI.

55+32 16'X12" corr. 14'

53+95 CEI. 29'

495 13<sup>E</sup> 20<sup>E</sup> 15" CONC.

52+06 17' 20'X12" corr.

+86 CEI 28'

+86 rail fence ends 26'

+70 19ft post rail fence 26'

57 15'X12" corr. 12'

51+41 19ft post rail fence end 26'

+67 27' CEI

50+37 rail fence beg. 26'

+92 16' 10"X18" corr.

49+32 16'X12" corr. 14'

48+66 28' CEI

+70 27<sup>E</sup> CEI

+33 no pipe (Needs 12")

47+11 15'X12" corr. 14'

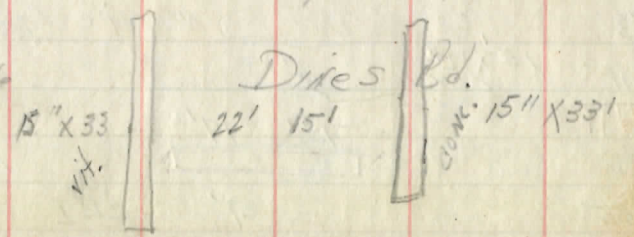
+86 15' 17' 15' CONC.

+65 27' CEI

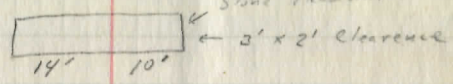
+43 CEI 29'

E W

56+43 23' short <sup>ping? 20' x 16'</sup> lawn tree row  
 +93 CEI 28'  
 57+16 36' x 12" cpr. 15'  
 58+17 28' Apple 13" (also 4 tree row)  
 +25 CEI 28'  
 +70 19' rock wall 6' 9"  
 +79 28' Buckeye 22"  
 59+02 28' Buckeye 36"  
 +30 27' map. 18"  
 +44 27' map. 24"  
 +60 18' stone wall bench  
 +60 25' x 10" east iron 15'  
 +66 16' 6" square tile vit 32'  
 +76 18' slate wall short  
 +89 29' CEI  
 60+01 CEI 33'  
 61+40 30' CEI  
 +40 29' end tree row  
 62+90 29' CEI



E W

63+35 30' Row of small Pines ↓  
 63+44 O.B.T. 29.5'  
 64+49 O.B.T. 29'  
 64+81 28.5' End of Pine Row ↑  
 64+88 28.5' CEI.  
 64+97 15' 15' 12" x 16' Corr.  
 65+54 O.B.T. 29'  
 65+91 Stone Culv.   
 66+88 29' CEI.  
 66+91 O.B.T. 29.5'  
 68+36 O.B.T. 28.5'  
 68+91 29' CEI.  
 69+25 17' 21' 6" steel 12" Conc. x 52.5'  
 69+70 19' 12" Cast Iron  
 69+76 O.D.T. 28'  
 69+82 27.5' End of Pipe  
 70+91 29' CEI.  
 71+19 O.B.T. 28'  
 72+55 O.B.T. 27'  
 72+80 28' CEI  
 72+87 14' 14' 12" Conc x 25'  
 73+96 O.B.T. 29'  
 74+91 26' Mull, Rise Hedge →  
 74+93 29' CEI

H. Patterson  
P. Young  
D. Ridenour

Parkin Road  
X Sec. Chag. River

B.M.	9.20	109.20		100.00
T.P.	10.11	111.70	7.61	101.59
T.P.	9.52,	119.32	1.90	109.80
0+0				111.62 ✓
T.P.	1.09	108.97	11.44	107.85
+50				106.27 ✓
1+0				102.87 ✓
+50				101.37
T.P.	3.49	104.16	8.30	100.67
2+0				100.66
3+0				100.16
4+0				99.16
5+0				99.96
T.P.	9.12	109.40	3.75	100.28
E. Side Bridge				104.30
6+0				104.90
W. Side Bridge				100.00
B.M.	9.71	109.71	9.41	99.99
7+0				105.91

SPK N.E. Root 10" Elm 40' SE of SEK Bridge  
410' W. of 34" Sycamore

		S.		E.		N.			
0.6	0.6	8.4	7.9	7.7	8.2	8.7	7.9	2.2	5.3
<u>30</u>	<u>22</u>	<u>10</u>	<u>9</u>		<u>9</u>	<u>10</u>	<u>11</u>	<u>19</u>	<u>30</u>
1.5	3.9	3.4	3.7	3.0	2.7	3.4	5.1	7.3	10.9
<u>30</u>	<u>20</u>	<u>15</u>	<u>11</u>	<u>9</u>		<u>11</u>	<u>15</u>	<u>22</u>	<u>30</u>
8.3	7.6	7.2	6.3	6.1	6.7	8.4			9.9
<u>30</u>	<u>17</u>	<u>15</u>	<u>8</u>		<u>11</u>	<u>16</u>			<u>30</u>
7.0	7.1	7.5	7.8	7.6	8.2	8.0	9.6		9.8
<u>30</u>	<u>25</u>	<u>12</u>	<u>10</u>		<u>11</u>	<u>17</u>	<u>18</u>		<u>30</u>
4.3	4.1	Drive	3.9	3.5	3.8	3.2	2.6		4.0
<u>30</u>	<u>24</u>		<u>9</u>		<u>12</u>	<u>21</u>	<u>25</u>		<u>30</u>
4.5	3.8	3.7	4.5	4.0	4.6	5.1	5.1		5.2
<u>30</u>	<u>24</u>	<u>15</u>	<u>11</u>		<u>12</u>	<u>17</u>	<u>21</u>		<u>30</u>
6.3			5.5	5.0	5.4	6.0	6.6		6.2
<u>30</u>			<u>12</u>		<u>13</u>	<u>15</u>	<u>22</u>		<u>30</u>
4.9	4.9	6.3	5.1	4.2	4.7	6.4	6.6		5.5
<u>30</u>	<u>20</u>	<u>13</u>	<u>9</u>		<u>14</u>	<u>13</u>	<u>21</u>		<u>30</u>
				4.6					
				4.5					
9.6	8.8	4.9	4.4	3.8	4.9		6.4		
<u>30</u>	<u>22</u>	<u>18</u>	<u>12</u>		<u>19</u>		<u>30</u>		



		130.15		
T.P.	0.20	118.57	11.75	118.37
T.P.	2.58	109.63	11.82	106.75
B.M.			9.63	100.00

W. edge Bridge

7.25

I.B.H. 6'

SPK SW. side  
30" Trip Elm. 8'

30.12

Caves Rd.  
Topo

D. Pidenour  
D. Moss  
S. Smith

Aug. 14, 1961  
Warm + Clear

52

E

W

W

75+44	O.B.T.	26'	
76+58	12" Ash	27'	
76+73	12" Cherry	27'	
76+93	CEI	25.5'	
76+93		29'	CEI
77+20	Lilac Bush	24'	
78+00		29'	6" Wood Post
78+11		15.5'	12" Corr. x 20.5'
78+18		29'	6" Wood Post
78+32	O.B.T.	27'	
78+77	12" Corr x 25'	14.5'	
78+87	4x4 Wood light Post	27.5'	
78+92		29'	CEI
79+14		32'	10" Cherry
79+71	O.B.T.	29.5'	
80+37		26'	Mult. Rose Hedge ↓
80+37		29'	Woven Wire Fence ↓
80+58		26'	End of Hedge End of Fence ↗
80+76		15.5'	10" Corr. x 20" (paved)
80+95		28.5'	CEI
81+06	O.B.T.	28'	
82+03		25'	Start of Hedge ↘
		26'	Start of Fence ↓
82+29		27'	End of Hedge ↑

East      West

82+55	O.B.T.	28.5'	
82+94		29'	CEI and Fence <sup>Woven</sup> ↑
83+02	(in conc.) 3" Metal Sign Post	14'	
83+16	12" Corr. x 18'	14.5'	Repaired
83+99	CEI	29'	
84+34	12" Corr. x 20.5'	13.5'	
85+00		30'	CEI and Fence ↓
85+06	12" Corr. x 20'	14'	
85+37	O.B.T.	27'	
85+39		29'	End of Fence ↑
85+48		10'	N. Pipe
85+81	Repaired	23'	10" Pipe
86+02	12" Corr. x 20'	15.5'	
86+28		19'	Pine Shrubs
86+53		19'	
86+79	O.B.T.	27.5'	
86+97		29'	CEI
87+02		18.5'	9" Pine
87+15		13.5'	12" x 19.5' CAST IRON
87+24		29'	Woven Wire Fence ↓
87+48		29'	10" Cherry
87+53	CEI	28'	
87+78		29.5'	14" Cherry ↓
87+84		29.5'	10" Elm ↓

East      West

88+24	O.B.T.	29'	
88+52		30'	10" Elm
88+54		30'	8" Elm
88+99		28'	CEI
89+00	4" Pine Shrub	22'	
89+43		21' 19'	24" Conc. Cross pipe
89+59		29'	Row of Trees and Fence ↓
89+64	CEI	29'	
90+15	O.B.T.	29'	
90+63		28'	18" Twin Cherry in Row ↑
90+63		28'	and Woven Wire Fence ↓
90+72	No Pipe	22'	
91+00		28'	CEI and Fence ↓
91+10	CEI	30'	
91+12		28'	10" Cherry ↓ Fence
91+73		29'	20" Twin Cherry End of Row
92+75	12" Corr. x 18'	15.5'	
92+81	O.B.T.	28'	
92+84		29'	End of Fence ↗
92+98		30'	CEI
94+22	O.B.T.	28.5'	
94+26	4" drain pipe	15'	
94+98		28'	CEI
95+16		12'	12" Corr. x 28' & Brenner Drive

East & West

95+17 4" steel Post 22'

95+26 12" Corr. x 16" 14'

95+69 O.B.T. 28.5'

95+87 4" T.I.P. Pipe 15'

96+98 29' CEI

97+23 CEI. 29'

97+76 22" Maple 27'

98+10 8" Corr. x 39.5' 15'

98+94 O.B.T. 28.5'

98+97 29' C.E.I.

100+04 18" Conc. Crossover Pipe  
18 19

101+57 CEI 28'

101+72 28.5' CEI

101+92 James Drive

101+99 12" Corr. x 21' 14.5'

102+16 23.5' 4x4 wood Sign Post

102+60 Asphalt drive 24.5' Pipe

102+85 29' CEI.

102+26 CEI 28'

103+79 10" Cast Iron x 17.5' 13.5'

103+90 3" Shrub 19'

103+98 29' CEI

104+76 3" Shrub 25.5'

104+87 O.B.T. 28.5'

East & West

105+22 23' 14" Locust

105+92 30' CEI

106+35 15" Conc 17 16 15" steel Crossover Pipe

106+45 O.B.T. 28'

106+88 17' 10" Corr. x 24'

107+94 CEI 29'

107+94 29' CEI

A. Patterson  
P. Young  
D. Ridenour

Cedar Road  
To Po

+12	-20'	Q8" Maple
15+01	-21'	Q 10" Elm
+86	-20'	Q8" Elm
+84	-20"	Q10" Elm
+79	-19'	Q9" Elm
+64	-21'	Q10"
+63	-20'	Q10" Elm
+58	-25'	O CEI
+50	-18'	Q Quod Maple
+40	-18'	Q10" Elm
+30	-21'	Q10" Maple
+11	-16.5'	Q12" Cherry
+07	-22'	Q10 Maple
14+02	-21'	Q10" Twin Elm
+82	-18'	Q9" Elm
+63	-18'	Q15" Elm
+46	-19'	Q15" Elm
+17	-17'	Q15" Elm
13+00	-15.5'	Q <sup>50"</sup> Twin Elm
+90	25'	O CEI
+80	15'	Q 15" Elm
+70	11'	Q16" Twin Maple
+62	19'	Q 10" Elm
Westchester trail	11'	Q 10" Elm
12+61	23'	Q 10" Elm

Brush

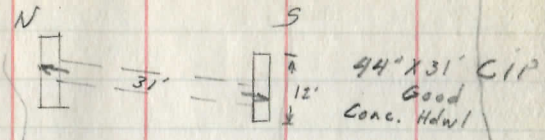
Brush

12" X 61' C.I.P.

12+61 Rd N.

E

Station	Notes	Distance	Tree/Feature
+80		31'	44" X 31" CIP Good Conc. Hdwl
+28			28' @ 15° T. Elm
19+00	Clump 15" Elm E	29'	
+29			27' 0 CFI
+14	10" Elm E	25'	
18+06	10" Elm E	21'	
17+96			20' @ 30° Cherry 10" X 25" Good Conc. Post
+49	Brush		Drive
+33		25.5'	@ 12" Elm
+30		26'	0 CFI
+15	No Post		Drive
+10	14" Drive	18.5'	@ 10" Elm
16+02		14'	@ 14" Trip Elm
+96		24'	@ 12" Elm
+93		25'	@ 13" Elm
+90		22.5'	@ 8" Elm
+84		20'	@ 12" Elm
+70		19'	@ 10" Twin Elm
+54		20'	@ 16" w Cherry Good
+49		20'	@ 9" Maple
+32		25'	@ 12" Twin Elm
+29		21'	@ 15" Twin Elm
15+20		23'	@ 12" Elm



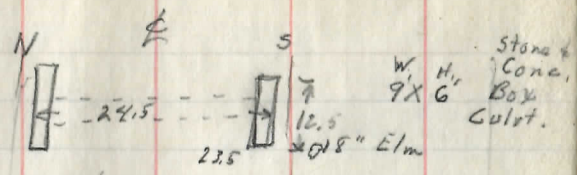
Brush

Brush

No Post  
14" Drive

Brush

15 X 21"  
Good Conc. Post



- 25+08
- 25+04
- 79B
- +80
- +69
- +58
- +52
- +30
- 24+13
- 23+52
- 23+41
- 176
- +46
- +40
- +33
- +12
- 2210
- 21+29
- +27
- 20+03

18" Oak 30'  
 16" Maple 23.5'

- 23.5
- 12.5
- 18" Elm
- 24' E24" Oak
- 22' D10" Dead Elm
- 22' D15" Dead Elm
- 28' D20" Elm
- 27' O CEI
- 8.75
- 21' 31" Elm
- Brush
- 8.75
- Guard Rail
- 21' 30" Quad Oak
- 28' T. Cherry
- 21' T. Oak
- 29.5' D 25" Maple
- 29.5' O CEI

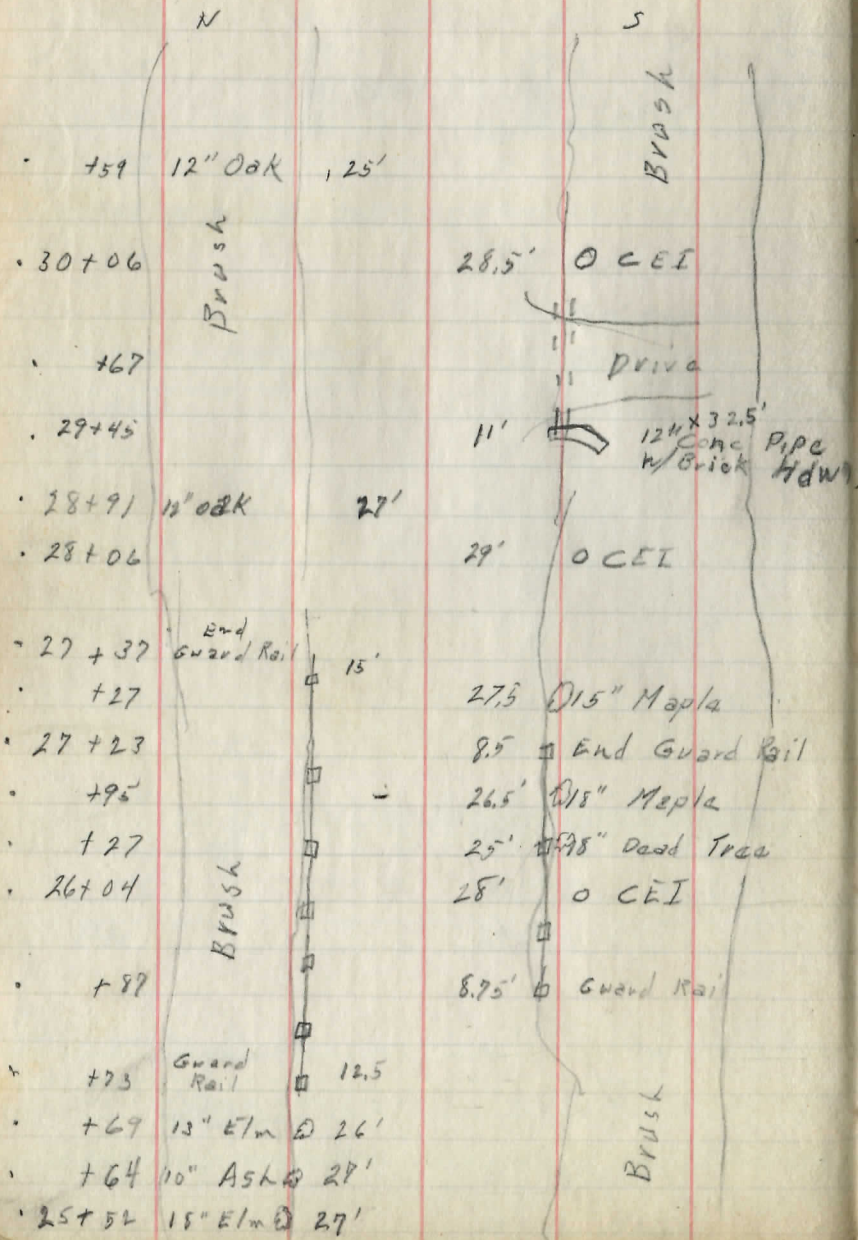
Brush

Brush

18" x 45.5" Conc

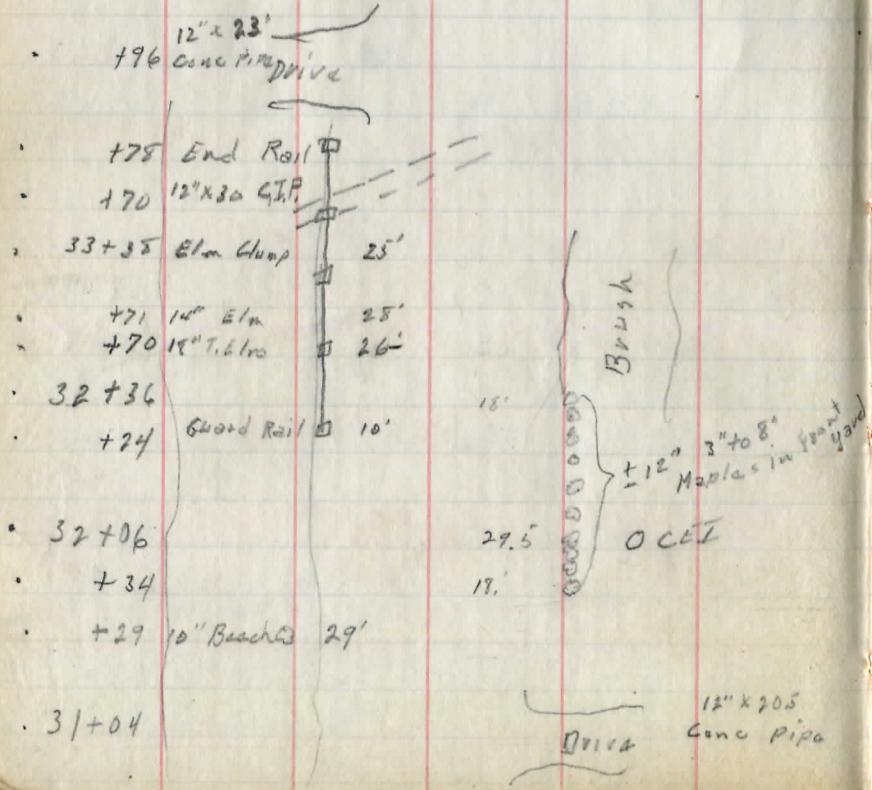
West Georgia Trail

- 25' O CEI
- 29' D16" Maple



N

S



- +37 30' C.E.I
- 80 +02 29' 15" Cherry
- +54 29' x T. Cherry
- +29 29' 15" Cherry
- 79 +19 29' 15" Ash
- +95 15' X 40.5' C.I.P. Cross Rd Culvt. Rusted thru bottom
- +85 Int. Caves Rd N. & S.
- 78 +61 28' 0 C.E.I

Brush

Brush

Brush

- +85 12" X 24" Asphene Drive
- +60 29' 0 C.E.I
- 76 +05 6" Drain Tile 7'
- +85 12" X 24" Conc Drive 6.3'
- 75 +0

83+99 12" Ash 32 29 C.E.I.  
 +92 15" Ash 33  
 +45 29' 20" Oak  
 +32 BRUSH 29' 15" Quod Ash

20" Ash  
 26" Beach

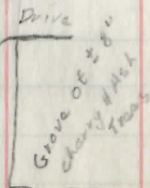
+25  
 +23  
 +22

27'

15' + + + Steel Guard rail

Drive

30' to 60'



83+0

30' 0 C.E.I.

Row of trees 20' or 6'

+42

BRUSH

82+15

+68 18" Maple 31'

+47

30' 15" Cherry

+47

31' 8" "

+45

30' 12" "

+26

30' 15" cherry

+18

29' 12" cherry

81+06 18" Maple 36'

80+97

BRUSH

29' 15" Ash

BRUSH

• 128+25 C&I 28'

• 128+20 33' 8" Maple

• +65 24' 3" Pine

• +57 17' 5' Rock Garden

• 127+26 21' 18" Maple

• +97 22.5' 10" Maple

• +69 23' 13" Cherry

• +37 24' 10" Maple

• +24 C&I 0 29'

• 126+14 24' 15" Maple

• +55 Marilyn 15' Dr 10" x 34" Conc.

• +45 24' 15" Maple

• 125+38 <sup>Driv</sup> 12' x 6' C&I 14.5' 21' 15" Maple

• +54 C&I 0 29'

• +24 <sup>Conc.</sup> 10" x 20 15'


• +12 2" B. Spruce 22

• 124+0 10" T. Elm 15'

•	+30	Fence X C.E.I.	32.5' 29'	17'	Drive <sup>Block-top</sup> 12" X 20' G.P.
•	+15				8" Spruce
•	132+0			25.5'	3" Arborvita
•	+93			31.5'	12" Pine
•	+67			34'	8" Pine
•	131+46			27'	15" Ash
•	+96			36'	54" Beech
•	+61				14" Stump
•	+48			23'	12" Elm
•	+35			23'	15" Stump + tree
•	+29	C.E.I.	29'		
•	+18	15" Maple	16.5'		
•	130+12	24" Stump	22'	25'	24" Stump & shoots Blind
•	+78			24'	18" Elm
•	127+52		15' $\frac{11}{2}$	13.5'	culvt 4.5 X 4.5' Conc + Stone
•	+89			27'	8" Maple
•	+82			17'	Drive 10" X 24.5' conc
•	128+58	Brush		29'	Rock Garden C.E.I.

	X			
	X			
+62	X		17'	Hedge row
+47	X		15'	Drive 12" x 29' Vit. Tile
+29	X		22'	20" Maple x x x x
137+15	X	CEI	24'	
+79	X		17' $\frac{17}{16}$ = 1.0625	3' W x 45" D Stanchion Conc
	X			
	X			
136+06	X		26'	22" Ash
	X			
+68	X	Fence CEI	26' 25'	
135+43	X		26.5'	Fence
	X			
+95	X		23'	24" Maple
+70	X		28'	12" Tulip
	X			Brush
+15	X		30'	13" Tulip
134+12	X	Fence CEI	26' 24.5'	
+83	X		26'	18" Maple
133+69	X		25.5'	40" Elm
	X			Brush
+91	X		25'	24" Maple
+60	X		25'	CEI
132+43	X		24'	20" cherry
	X			

141+13 & Intersection SR 306

+80		28.5'	3" Pine
+63	Edge Post, 		
+53		24.5'	15" Maple
+30		23.5'	16" Maple
140+03	25'	23'	15" Maple
+83			Drive ← 12" x 4" CIP Conc.
+77		23'	13" Maple
+68		15'	Drive ←
+52	-	23'	20" Elm
139+42		21'	End Hedge & Fence X X X
+94	End Fence X X V X	27'	
+35	X	26'	10" Pine
+36	X	20'	Hedge
	X	21'	Juniper
	X	25'	CEI
135+23	CEI	24.5'	

11/21/59

X sec

Cool 40°

H Patterson  
I. Kingston  
G. Diedrich

Cedar Rd

BM #1 9.27 109.27 100.00 I.P. in

1+00 103.77  
103.67

Driva 15" x 20' CMP Good 24' off Lt 0+67

2+00 105.17

T.P. 11.57 119.50 1.34 107.93

3+00 108.10  
108.00

4+00 111.80

5+00 115.10  
115.00

T.P. 10.23 128.05 1.68 119.82

6+00 117.65

7+00 120.05  
119.85

8+00 122.55

+12 10" x 20' Conc. 18' off Lt

TP 11.22 138.93 0.34 127.71

9+00 126.23  
126.83

TP 6.27 141.54 3.36 135.57

BM #2 +.31 142.15 Hort.

BM #5 2.66 181.82 179.16 R.P.

30+00 173.12

Note: Changed to match Profile Elev. (66)  
See F.B. 139 pp. 60 startN E S  
Mon box Int. County Line Rd & Cedar

<del>5.8</del> 30	<del>5.9</del> 21.5	<del>7.9</del> 17	<del>5.4</del> 13	5.5 5.5	5.8 5	6.9 9.5	6.3 12	7.8 30
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4.1 30	4.1 24	4.5 15.5	4.3 15	3.8 3	4.1	4.3 5	6.2 7	4.1 10	4.2 30
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10.5 <del>11.1</del> 31	9.2 <del>9.3</del> 23	12.1 <del>12.2</del> 17	11.6 <del>11.7</del> 14	11.3 <del>11.4</del> 4	11.4 <del>11.5</del>	11.6 <del>11.7</del> 5	12.2 <del>12.3</del> 8	11.1 <del>11.2</del> 9	8.6 <del>8.7</del> 22	8.5 <del>8.6</del> 30
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5.5 30	6.5 22	9.1 17	8.0 14	7.5 4	7.7	8.0 6	8.5 7	6.8 10	4.6 20	5.2 30
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8.8 <del>8.9</del> 32	3.4 <del>3.5</del> 23	6.2 <del>6.3</del> 17	4.9 <del>5.0</del> 14	4.3 <del>4.4</del> 3.5	4.4 <del>4.5</del>	4.8 <del>4.9</del> 6	5.2 <del>5.3</del> 8	3.5 <del>3.6</del> 12	3.6 <del>3.7</del> 30
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10.1 30	10.2 24	11.3 17.5	10.9 18.5	11.3 5.5	10.4	10.5 4	11.4 6	10.9 11	10.7 30
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7.7 <del>7.8</del> 31	8.3 <del>8.4</del> 15	8.9 <del>9.0</del> 16	8.3 <del>8.4</del> 14	7.9 <del>8.0</del> 4	8.0 <del>8.1</del>	8.2 <del>8.3</del> 5.5	8.8 <del>8.9</del> 5	8.3 <del>8.4</del> 10	9.6 <del>9.7</del> 30
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4.3 30	5.3 15.5	7.1 16	5.7 12.5	6.5 3	5.5	5.7 6	6.5 9	5.1 12	5.8 30
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10.1 <del>10.2</del> 30	10.8 <del>10.9</del> 21	14.5 <del>14.6</del> 14.5	12.9 <del>13.0</del> 11	12.6 <del>12.7</del> 3	12.7 <del>12.8</del>	12.9 <del>13.0</del> 5	13.8 <del>13.9</del> 5.5	11.9 <del>12.0</del> 13	11.6 <del>11.7</del> 30
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spk. N. side C.E.I. #578627

spk. S. side 28" Beech 30' Lt. &amp; Sta. 31+50

9.3 30	8.2 16	9.6 11	8.7	9.7	9.1 8	9.5 11	5.9 17	4.8 30
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		181.82			176.82
31+00					179.42
+06	12" X 20'	CONC.	12' over 4 ft	Good	179.32
32+00					179.69
T.P.	7.55	187.24	2.13		179.84
33+00					179.64
34+00					179.94
35+00					181.94
					181.84
T.P.	12.00	197.63	1.61		185.63
36+00					186.13
					186.53
37+00					190.73
					190.53
T.P.	7.99	203.37	2.25		195.38
38+00					195.37
					195.27
39+00					198.07
40+00					199.67
					199.57
					199.47
T.P.	6.52	207.24	2.65		200.72
B.M. #6			7.90		199.34
42+00					201.34
					201.04

Hort.

N				S			
5.4	3.6	5.4		5.1	5.2	Drive	3.1
<del>3.0</del>	<del>1.7</del>	<del>1.2</del>			<del>5</del>		<del>3.0</del>
6.4	2.8	3.0	2.7	2.4	3.0	3.0	
<del>6.4</del>	<del>2.8</del>	<del>3.0</del>	<del>2.7</del>	<del>2.4</del>	<del>3.0</del>	<del>3.0</del>	0.0
3.0	1.5	1.3	1.9		1.6	1.2	2.1
							up 2' up 1'
14.9	12.1	7.9		7.4	7.8	8.3	6.9
<del>15.1</del>	<del>12.1</del>	<del>8.1</del>		<del>7.4</del>	<del>8.0</del>	<del>8.5</del>	<del>7.1</del>
<del>3.0</del>	<del>1.6</del>	<del>1.0</del>			1.1	1.3	1.6
							3.0
8.0	10.3	7.5	7.8	7.3	7.8	5.6	6.5
<del>3.0</del>	<del>1.6</del>	<del>1.2</del>	<del>7.8</del>		<del>1.0</del>	<del>1.2</del>	<del>1.6</del>
5.8	5.4	6.0	6.0	5.8	5.7	6.8	5.6
<del>5.8</del>	<del>5.4</del>	<del>6.0</del>	<del>6.0</del>	<del>5.8</del>	<del>5.7</del>	<del>6.8</del>	<del>5.6</del>
3.0	1.8	1.4	1.2		1.0	1.2	1.5
							2.9
12.4	14.1	12.1		11.5	11.8		11.2
<del>12.4</del>	<del>13.7</del>	<del>11.7</del>		<del>11.5</del>	<del>11.8</del>	Drive	<del>11.2</del>
3.0	1.3	1.9			1.9		3.0
4.6	4.4	7.8	7.4	6.9	7.4	8.0	5.0
<del>4.6</del>	<del>4.4</del>	<del>5.0</del>	<del>7.4</del>	<del>7.1</del>	<del>7.4</del>	<del>8.0</del>	<del>5.0</del>
3.0	1.1	1.1	1.9		1.9	1.1	1.7
5.2	5.2	8.6		8.0	8.6	9.1	5.2
<del>5.2</del>	<del>5.2</del>	<del>8.6</del>		<del>8.0</del>	<del>8.6</del>	<del>9.1</del>	<del>5.2</del>
3.0	1.9	1.3			1.9	1.1	1.6
							3.0
4.5	4.1	5.7	5.3	5.3	5.8	3.2	2.7
<del>3.0</del>	<del>1.7</del>	<del>1.2</del>	<del>2</del>		<del>1.0</del>	<del>1.7</del>	<del>3.0</del>
4.7	4.4	5.0	4.2	3.7	3.8		2.0
<del>3.0</del>	<del>1.6</del>	<del>1.4</del>	<del>1.2</del>	<del>2</del>	<del>1.9</del>		<del>3.0</del>
6.3	4.8	4.0	3.8	3.8	4.5	5.6	5.2
<del>6.3</del>	<del>4.8</del>	<del>4.0</del>	<del>3.8</del>	<del>3.8</del>	<del>4.5</del>	<del>5.6</del>	<del>5.2</del>
3.0	1.4	1.2	1.1		1.0	1.2	1.5
							3.0
5.9					5.9	6.6	7.4
<del>3.0</del>					<del>6.2</del>	<del>7.1</del>	<del>6.8</del>
					1.0	1.2	1.4
							6.2

spk. SE. side Quad Ash Clump 72' Lt. Sta. 41+55

		207.24		203.24	
43101				203.04	
T.P.	8.54	213.68	2.10	205.14	
44100				205.68	
45100				208.38	
				208.28	
46100				109.68	
47100				210.78	
				210.58	
48100				211.18	
B.M. + T.P.	5.33	217.01	2.00	211.69	Hort.
49100				211.21	
50100				211.21	
51100				211.91	
				211.71	
52100				212.61	
				212.41	
53100				212.91	
				212.71	
54100				213.31	
T.P.	4.92	218.71	3.22	213.79	
55100				213.91	
				213.71	

2.5	3.2	5.4	4.4	8.9	4.0	4.6	4.7	2.9	2.1
<del>3.1</del>	<del>3.2</del>	<del>5.4</del>	<del>4.4</del>	<del>8.9</del>	<del>4.0</del>	<del>4.6</del>	<del>4.7</del>	<del>2.9</del>	<del>2.1</del>
3.1	2.4	2.0	1.3	3		8	10	14	31
6.4	5.7	9.5	8.5		8.0	8.3	9.0	6.6	6.5
<del>3.0</del>	<del>2.2</del>	<del>1.5</del>	<del>1.1</del>			<del>1.0</del>	<del>1.2</del>	<del>1.5</del>	<del>3.0</del>
5.6	4.8	6.6	5.7		5.3	5.8	6.7	4.7	4.8
<del>5.6</del>	<del>4.8</del>	<del>6.6</del>	<del>5.7</del>		<del>5.3</del>	<del>5.8</del>	<del>6.7</del>	<del>4.7</del>	<del>4.8</del>
3.0	7.9	1.5	1.4			1.0	1.2	1.5	3.0
4.8	4.7	5.4	4.6		4.0	4.6	4.9	3.3	3.4
<del>3.1</del>	<del>1.7</del>	<del>1.5</del>	<del>1.3</del>			<del>1.0</del>	<del>1.1</del>	<del>1.4</del>	<del>3.0</del>
2.8	3.5	3.0	2.7	2.9	3.3	4.0	2.4	2.5	
<del>3.0</del>	<del>3.5</del>	<del>3.0</del>	<del>2.7</del>	<del>2.9</del>	<del>3.3</del>	<del>4.0</del>	<del>2.4</del>	<del>2.5</del>	<del>3.0</del>
3.1	2.7	3.8	2.9	2.5	3.2	3.6	2.3	1.9	
<del>3.1</del>	<del>2.7</del>	<del>3.8</del>	<del>2.9</del>	<del>2.5</del>	<del>3.2</del>	<del>3.6</del>	<del>2.3</del>	<del>1.9</del>	<del>3.0</del>
3.0	2.0	1.6	1.5		2.3	3.7	1.4	1.4	3.0
spk. S. side 15" Trip White wood 33' Lt. Sta. 49+30									
7.1	6.7	7.1	6.6	5.8	6.6	7.2	6.0	6.0	
<del>3.1</del>	<del>1.7</del>	<del>1.4</del>	<del>1.1</del>		<del>1.0</del>	<del>1.2</del>	<del>1.6</del>	<del>3.0</del>	
5.9	6.6	7.1	6.2	5.8	6.4	7.2	5.7	5.9	
<del>3.0</del>	<del>1.9</del>	<del>1.3</del>	<del>1.0</del>		<del>1.2</del>	<del>1.4</del>	<del>1.7</del>	<del>3.0</del>	
5.2	5.3	5.8	5.8	5.1	5.1	5.6	6.0	3.7	4.8
<del>3.0</del>	<del>1.7</del>	<del>1.1</del>	<del>1.5</del>	<del>1.1</del>	<del>1.4</del>	<del>1.3</del>	<del>1.5</del>	<del>1.8</del>	<del>3.0</del>
5.9	4.8	5.1		4.4	4.9	5.0	5.3	3.5	3.5
<del>3.0</del>	<del>1.1</del>	<del>1.0</del>		<del>1.0</del>	<del>1.6</del>	<del>1.3</del>	<del>1.5</del>	<del>1.8</del>	<del>3.0</del>
4.8	4.6	5.3	4.3	4.1	4.0	4.9	4.3	4.3	
<del>3.0</del>	<del>1.2</del>	<del>1.1</del>	<del>1.7</del>	<del>1.3</del>	<del>1.4</del>	<del>1.5</del>	<del>1.8</del>	<del>3.0</del>	
3.8		3.8	4.6	4.0	3.7	3.6	4.4	3.1	3.2
<del>3.0</del>		<del>1.3</del>	<del>1.0</del>	<del>1.7</del>	<del>1.3</del>	<del>1.3</del>	<del>1.5</del>	<del>1.8</del>	<del>3.0</del>
5.8	4.9	6.1	5.4	4.8	4.7	5.4	5.8	4.4	4.6
<del>3.0</del>	<del>1.3</del>	<del>1.0</del>	<del>1.7</del>	<del>1.3</del>	<del>1.4</del>	<del>1.5</del>	<del>1.6</del>	<del>2.0</del>	<del>3.0</del>

218.71

56+00

213.91

57+00

214.31

58+00

214.81

59+00

213.71

B.M. #8

1.61

217.62

2.70

216.01

Hort. spr.

60+00

210.72  
210.62

61+00

207.42  
207.22

T.P.

2.51

208.91

11.72

205.90

62+00

204.11  
203.91

63+00

201.81  
201.61

64+00

199.31  
199.21

T.P.

65+00

4.17

202.58

10.00

198.41  
197.38  
197.18

$\frac{5.4}{30}$

$\frac{5.4}{13}$

$\frac{6.0}{11}$

$\frac{4.9}{5}$

4.8

$\frac{4.7}{4}$

$\frac{5.4}{12}$

$\frac{5.7}{14}$

$\frac{5.0}{16}$

$\frac{4.7}{30}$

$\frac{5.5}{30}$

Drive

$\frac{4.5}{5}$

4.4

$\frac{4.5}{12}$

$\frac{5.3}{15}$

$\frac{4.5}{17}$

$\frac{4.7}{30}$

$\frac{3.1}{30}$

$\frac{4.0}{13}$

$\frac{5.0}{16}$

$\frac{4.2}{8}$

3.9

$\frac{3.9}{3}$

$\frac{4.9}{14}$

$\frac{5.5}{16}$

$\frac{3.1}{17}$   
 $\frac{3.0}{30}$

$\frac{3.5}{30}$

Drive

$\frac{5.0}{5.5}$

5.0

$\frac{5.0}{6}$

$\frac{5.6}{15}$

6.4

$\frac{2.9}{12}$

$\frac{2.7}{30}$

s. side C.F.T. # 593614 31 Lt. Sta. 58+81

$\frac{5.6}{30}$

$\frac{5.5}{14}$

$\frac{8.0}{9}$

$\frac{7.2}{7}$

$\frac{6.9}{4}$

$\frac{6.8}{14}$

$\frac{7.6}{15}$

$\frac{8.3}{21}$

$\frac{5.1}{21}$

$\frac{4.5}{30}$

$\frac{8.7}{30}$

$\frac{10.0}{14}$

$\frac{11.5}{11}$

$\frac{10.7}{9}$

$\frac{10.2}{7.5}$

$\frac{10.2}{12}$

$\frac{10.9}{17}$

$\frac{11.8}{18}$

$\frac{9.4}{18}$

$\frac{8.8}{30}$

$\frac{3.1}{30}$

$\frac{4.1}{11}$

$\frac{5.5}{10}$

$\frac{4.5}{7}$

$\frac{4.3}{4}$

$\frac{4.3}{13}$

$\frac{4.8}{16}$

$\frac{5.8}{20}$

$\frac{2.2}{20}$

$\frac{2.0}{30}$

$\frac{5.8}{30}$

Drive

$\frac{6.6}{5}$

$\frac{6.6}{5}$

$\frac{6.6}{14}$

$\frac{7.2}{15}$

$\frac{7.9}{17}$

$\frac{7.0}{17}$

$\frac{6.9}{30}$

$\frac{8.1}{30}$

$\frac{8.2}{15}$

$\frac{10.5}{16}$

$\frac{9.4}{7}$

$\frac{9.1}{5}$

$\frac{9.1}{13}$

$\frac{9.8}{15}$

$\frac{10.3}{15}$

$\frac{9.2}{15}$

$\frac{9.6}{30}$

$\frac{4.6}{30}$

$\frac{4.6}{13}$

$\frac{6.2}{10}$

$\frac{5.6}{9}$

$\frac{5.2}{6}$

$\frac{5.2}{14}$

$\frac{5.9}{16}$

$\frac{6.3}{19}$

$\frac{5.0}{19}$

$\frac{5.7}{30}$

12-5-59

C201

BM #11	2.12	249.70		247.58
T.P.	0.26	237.96	12.00	237.70
T.P.	0.46	226.59	11.83	226.13
T.P.	0.73	216.34	10.98	215.61
86+0				210.24
				201.45
87+0				201.44
T.P.	0.75	205.58	11.51	204.83
T.P.	2.28	197.82	10.04	195.54
88+0				193.14
				193.02
T.P.	1.05	188.13	10.94	187.08
89+0				184.83
				184.43
T.P.	1.78	178.46	11.45	176.68
90+0				175.76
				175.96
T.P.	2.07	169.44	11.09	167.37
91+0				167.34
92+0				160.40
				160.34
T.P.	1.39	161.08	9.75	159.69
93+0				157.08
BM #12			4.04	157.04
94+0				155.48
95+0				155.88
T.P.	8.34	163.93	5.49	155.59

N

S

2.2	2.4	6.0	6.8	6.1	5.7		6.5	7.5	6.4	7.9
<del>2.2</del>	<del>2.4</del>	<del>6.0</del>	<del>6.8</del>	<del>6.1</del>	<del>5.7</del>		<del>6.5</del>	<del>7.5</del>	<del>6.4</del>	<del>7.9</del>
30	29	17	18	19	4		5	7	8	30
7.0		16.0	15.1	14.5	14.7	15.1	15.7	14.8	14.0	14.6
30		18	16	5		1	6	8	20	30
1.0	1.7	6.3	4.8	4.6	4.8		5.5	4.7	5.2	
30	28	21	19	7			10	11	30	
	3.4	4.4	3.3	3.1	3.3					2.9
	<del>3.4</del>	<del>4.4</del>	<del>3.3</del>	<del>3.1</del>	<del>3.3</del>					<del>2.9</del>
	30	4	20	8						21
2.7	5.9	3.1	2.4	2.7	3.1	3.9	2.2	1.9		
<del>2.7</del>	<del>5.9</del>	<del>3.1</del>	<del>2.4</del>	<del>2.7</del>	<del>3.1</del>	<del>3.9</del>	<del>2.2</del>	<del>1.9</del>		
30	25	20	6	2.5	6	8	11	30		
0.8	5.0	4.2	2.2	2.0	2.1	2.3	3.3	1.7	3.8	3.0
36	29	21	16	5		7	9	13	20	30
8.3	10.6	10.0	9.0	9.1	9.1		9.7	13.3	14.6	
36	29	17	13	3			12	15	30	
5.0	4.3	5.7	4.2	4.0		4.4	6.0	6.9		
30	17	15	12			12	14	30		
7.3	6.8	6.3	5.8	5.6		6.4	7.2	6.0	6.7	
30	23	15	12			14	18	21	30	
6.7	6.3			5.2	5.9	6.9	5.6	6.1		
30	27				14	17	14	30		

70

163.93

96+0 157.03

97+0 159.33

T.P. 6.20 169.61 0.52 163.41

98+0 162.16 = 162.21  
162.01

T.P. 6.55 175.22 0.94 168.67

99+0 165.22

100+0 168.42  
168.62

101+0 170.72

T.P. 11.16 183.36 3.02 172.20

102+0 172.76

103+0 175.16

104+0 177.20  
177.26

105+0 178.86

106+0 181.30  
181.16

107+0

T.P. 6.75 177.91 2.20 181.16

BM #13 4.37 183.57

N

S

$\frac{8.4}{30}$   $\frac{7.6}{16}$   $\frac{8.2}{14}$   $\frac{7.6}{12}$  6.7  $\frac{8.0}{14}$   $\frac{8.8}{16}$   $\frac{7.3}{19}$   $\frac{6.2}{30}$

$\frac{5.0}{30}$   $\frac{5.4}{15}$   $\frac{6.3}{19}$   $\frac{5.4}{14}$  4.6  $\frac{5.1}{12}$   $\frac{6.0}{15}$   $\frac{3.9}{19}$   $\frac{2.5}{30}$

~~6.9~~  
~~30~~ Drive ~~7.4~~ ~~9.1~~ 3.5 3.0  
~~30~~ ~~23~~ ~~30~~

$\frac{8.4}{30}$   $\frac{16.3}{17}$   $\frac{11.3}{15}$   $\frac{10.8}{14}$  10.0  $\frac{10.7}{12}$   $\frac{11.7}{16}$   $\frac{5.1}{24}$   $\frac{4.4}{30}$

~~7.2~~ 7.1 7.9 ~~6.8~~ 6.8 7.4 8.4 6.5 6.9  
~~30~~ ~~15~~ ~~15~~ ~~3~~ ~~6.6~~ ~~13~~ ~~16~~ ~~21~~ ~~30~~

$\frac{6.0}{30}$   $\frac{5.4}{15}$   $\frac{4.5}{4}$  4.5  $\frac{5.3}{11}$   $\frac{6.3}{14}$   $\frac{4.2}{19}$   $\frac{3.1}{30}$

$\frac{9.7}{30}$   $\frac{10.1}{20}$   $\frac{12.6}{19}$   $\frac{11.1}{14}$   $\frac{10.6}{3}$  10.6  $\frac{11.4}{12}$   $\frac{12.1}{18}$   $\frac{8.0}{21}$   $\frac{7.0}{30}$

$\frac{7.8}{30}$   $\frac{8.0}{18}$   $\frac{9.6}{15}$   $\frac{8.6}{13}$  8.2  $\frac{9.1}{13}$   $\frac{10.8}{16}$   $\frac{9.3}{18}$   $\frac{8.3}{30}$

$\frac{6.8}{30}$   $\frac{6.9}{17}$   $\frac{7.7}{16}$   $\frac{6.5}{13}$  6.1  $\frac{7.8}{13}$   $\frac{8.5}{16}$   $\frac{7.6}{17}$   $\frac{7.2}{30}$

$\frac{3.7}{30}$   $\frac{4.5}{17}$   $\frac{5.4}{14}$  4.5  $\frac{3.5}{14}$   $\frac{5.6}{16}$   $\frac{4.5}{17}$   $\frac{4.5}{30}$

~~1.8~~ ~~30~~ ~~2.4~~ ~~2.0~~ ~~3.0~~ 2.2 1.8 1.3  
22 18 15 18 30

187.91

107+0				182.11
108+0				182.31
109+0				182.91
110+0				182.51
T.P.	7.10	189.60	5.41	182.50
111+0				182.80
				183.34
112+0				183.40
113+0				184.50
114+0				187.20
T.P.	7.75	195.60	1.75	197.85
115+0				189.60
				190.74
116+0				190.60
117+0				189.50
B.M.	8.00	197.43	6.17	189.43
119+0				188.73

$\frac{6.6}{30}$	$\frac{6.3}{16}$	$\frac{6.7}{14}$	5.8	$\frac{6.3}{12}$	$\frac{7.1}{14}$	$\frac{6.4}{16}$	$\frac{5.5}{30}$	
$\frac{5.5}{30}$	$\frac{5.2}{18}$	$\frac{6.1}{14}$	5.6	$\frac{5.7}{10}$	$\frac{6.3}{13}$	$\frac{4.1}{17}$	$\frac{4.2}{30}$	
$\frac{5.9}{30}$		$\frac{6.1}{16}$	5.0	$\frac{5.7}{12}$	$\frac{6.7}{15}$	$\frac{5.5}{17}$	$\frac{5.5}{30}$	
$\frac{6.9}{30}$	$\frac{7.4}{17}$	$\frac{6.2}{12}$	5.4	$\frac{5.7}{11}$	$\frac{6.6}{15}$	$\frac{6.0}{16}$	$\frac{6.9}{30}$	
$\frac{7.4}{30}$	$\frac{7.8}{20}$	$\frac{8.7}{17}$	$\frac{7.5}{10}$	6.8	$\frac{7.4}{12}$	$\frac{8.2}{15}$	$\frac{7.7}{26}$	$\frac{8.4}{30}$
$\frac{8.2}{30}$	$\frac{8.0}{17}$	$\frac{7.0}{12}$	6.2	$\frac{6.9}{11}$	$\frac{8.0}{15}$	$\frac{7.3}{17}$	$\frac{8.1}{30}$	
$\frac{4.8}{30}$	$\frac{4.6}{19}$	$\frac{6.0}{15}$	5.1	$\frac{5.5}{12}$	$\frac{6.0}{15}$	$\frac{4.8}{16}$	$\frac{4.6}{30}$	
$\frac{0.5}{30}$	$\frac{0.9}{20}$	$\frac{3.5}{15}$	2.3	$\frac{2.3}{12}$	$\frac{3.0}{16}$	$\frac{1.8}{14}$	$\frac{1.5}{30}$	
$\frac{3.8}{30}$	$\frac{3.4}{21}$	$\frac{6.5}{15}$	6.0		$\frac{7.1}{14}$	$\frac{5.7}{17}$	$\frac{4.8}{30}$	
$\frac{2.1}{30}$	$\frac{2.0}{20}$	$\frac{5.3}{14}$	5.0		$\frac{5.5}{15}$	$\frac{5.0}{16}$	$\frac{4.4}{30}$	
$\frac{6.7}{30}$	$\frac{7.3}{15}$		6.1			Drive	$\frac{6.3}{30}$	
$\frac{8.5}{30}$	$\frac{9.9}{18}$	$\frac{10.3}{15}$	$\frac{9.4}{13}$	8.7	$\frac{9.4}{13}$	$\frac{10.1}{16}$	$\frac{8.9}{19}$	$\frac{9.5}{30}$

197.43

120+0

189.66  
189.63

121+0

191.33

122+0

193.03  
192.73

123+0

195.03

124+0

196.53

125+0

197.53  
197.33

BM

8.00 189.43

BM #16

7.58 212.22

204.64

136+0

204.92

137+0

204.5

138+0

206.22

139+0

208.46  
208.32

F.P.

11.31 220.54 2.99 209.23

N

S

$\frac{7.4}{30}$

Road

7.8

$\frac{8.3}{11}$

$\frac{9.1}{15}$

$\frac{6.9}{19}$

$\frac{7.4}{31}$

$\frac{6.2}{30}$

$\frac{6.4}{20}$

$\frac{7.9}{15}$

$\frac{6.8}{16}$

6.1

Drive

$\frac{5.1}{30}$

~~5.0~~  
 $\frac{4.7}{30}$

~~5.2~~  
 $\frac{4.9}{19}$

~~7.1~~  
 $\frac{7.1}{16}$

~~6.0~~  
 $\frac{6.0}{13}$

~~4.4~~  
 $\frac{4.4}{11}$

~~4.9~~  
 $\frac{4.9}{15}$

~~6.0~~  
 $\frac{6.0}{19}$

~~4.9~~  
 $\frac{4.9}{30}$

~~5.1~~  
 $\frac{5.1}{30}$

$\frac{2.1}{30}$

$\frac{2.7}{15}$

$\frac{4.9}{15}$

$\frac{3.2}{11}$

2.4

$\frac{3.3}{13}$

$\frac{2.8}{18}$

$\frac{2.9}{30}$

$\frac{1.3}{30}$

$\frac{1.5}{15}$

$\frac{3.0}{15}$

$\frac{1.6}{12}$

0.9

$\frac{0.9}{2}$

$\frac{1.7}{12}$

$\frac{2.7}{15}$

$\frac{2.0}{17}$

$\frac{2.9}{30}$

~~0.2~~

~~0.0~~  
 $\frac{0.0}{12}$

~~1.6~~  
 $\frac{1.6}{16}$

~~0.3~~  
 $\frac{0.3}{8}$

~~-0.1~~  
 $\frac{0.1}{13}$

~~0.5~~  
 $\frac{0.5}{17}$

~~1.8~~  
 $\frac{1.8}{19}$

~~1.1~~  
 $\frac{1.1}{19}$

~~0.9~~  
 $\frac{0.9}{30}$

$\frac{7.0}{30}$

$\frac{7.7}{22}$

$\frac{8.8}{20}$

$\frac{8.2}{17}$

7.3

$\frac{8.0}{13}$

$\frac{8.6}{16}$

$\frac{8.0}{30}$

$\frac{10.0}{30}$

$\frac{10.8}{24}$

$\frac{11.5}{22}$

$\frac{11.4}{18}$

$\frac{8.6}{15}$

7.7

$\frac{8.0}{11}$

$\frac{10.8}{17}$

$\frac{11.9}{30}$

$\frac{6.6}{30}$

$\frac{6.8}{19}$

$\frac{7.2}{17}$

$\frac{6.6}{15}$

$\frac{6.0}{3}$

6.0

$\frac{6.6}{7}$

$\frac{7.2}{10}$

$\frac{7.2}{13}$

$\frac{7.3}{30}$

~~1.7~~  
 $\frac{1.7}{30}$

~~2.0~~  
 $\frac{2.0}{20}$

~~4.7~~  
 $\frac{4.7}{15}$

~~4.8~~  
 $\frac{4.8}{13}$

~~3.7~~  
 $\frac{3.7}{14}$

~~4.5~~  
 $\frac{4.5}{20}$

~~2.0~~  
 $\frac{2.0}{20}$

~~2.0~~  
 $\frac{2.0}{30}$

220.54

14010

211.94

14113

213.44

N

S

$\frac{5.2}{30}$

$\frac{6.0}{22}$

$\frac{9.5}{15}$

8.6

$\frac{8.9}{11}$

$\frac{9.3}{15}$

$\frac{8.3}{17}$

$\frac{7.6}{31}$

$\frac{11}{150}$

$\frac{2.2}{100}$

5.1

$\frac{10.3}{100}$

$\frac{12.4}{150}$



Patterson 9-11-59 Cedar Rd Sec A.B.B.  
 Young 58°  
 Amendola Brun Protifa Side Rds

BM #14 4.66 193.76 189.10

No Culvt. Shady Lane Sta 113+94 S Int. width = 54'  
 1+0  
 2+0  
 3+0

BM #15 5.59 195.07 189.48

Culvt. Dorothy Dr. Run N. Sta. 120+24 12" X 61' Conc  
 1+0  
 2+0  
 3+0

T.P. 9.12 203.37 0.82 199.25

Culvt. Marilyn Rd. Run S. Sta. 125+82 10" X 36.5' Conc  
 Cedar Acres Drive  
 1+0  
 2+0  
 3+0

No Culvt Marilyn Rd. Run N. Sta 125+82

1+0  
 2+0  
 3+0

E. Ditch 2.0 E 6.9 W. Ditch 8.4  
 7.3  
 9.2  
 10.5

E Inlet 5.9 E 4.8 W outlet 6.4  
 4.6  
 5.3  
 6.0

E Inlet 5.7 E 4.0 W outlet 6.6  
 4.6  
 6.4  
 6.5

E. Ditch 5.0 E 4.6 W. Ditch 5.8  
 4.4  
 3.8

BM #16	11.22	215.86	204.64
139+0			11.32 209.54
139+0		7.42	208.44
141+13.31	Int. SR3064 Cedar	0.46	215.40
BM #16		11.22	204.64

Caves Rd

1964 Reto  
Mon. Box  
Sat  
9/64

24" Buckeye  
3425  
58+79<sup>10</sup> spk S.W. side  
20" Buckeye 26<sup>18</sup>  
44.93  
Spk S. side  
CEI # 230571  
Spk S.W. Side

(58+78.62  
Obs STA 2014  
mon box fd)

34+97<sup>99</sup>  
CEI # 53356  
Spk. N. Side  
24<sup>13</sup>  
25<sup>12</sup>  
Spk N. Side  
13" Map  
Spk N. side  
16" Map

(34+97.69  
Obs STA 2014  
mon box fd)

20+19<sup>28</sup>  
15" Ash  
29.28  
Spk N. Side  
42<sup>13</sup>  
CEI # 531181  
Spk SW side

(20+18.77  
Obs STA 2014  
mon box fd)

9+39<sup>66</sup> drive  
ME  
Osage  
28.00  
29.00  
CEI # 531175

(9+39.66  
Held 2014  
Mon Box Fd)

Caves Rd. 1964 Ref.

STA, 107+20.64

Obs 2014  
mon box fd.  
original pipe?

INT of caves + fairmount

83+60

CEI

28<sup>98</sup>

11<sup>98</sup>

50<sup>85</sup>

SW crack in  
Lamp Post

⊗ Tel. pole

82+98.04

Obs STA 2014  
mon box fd  
I.P. bent took at bend

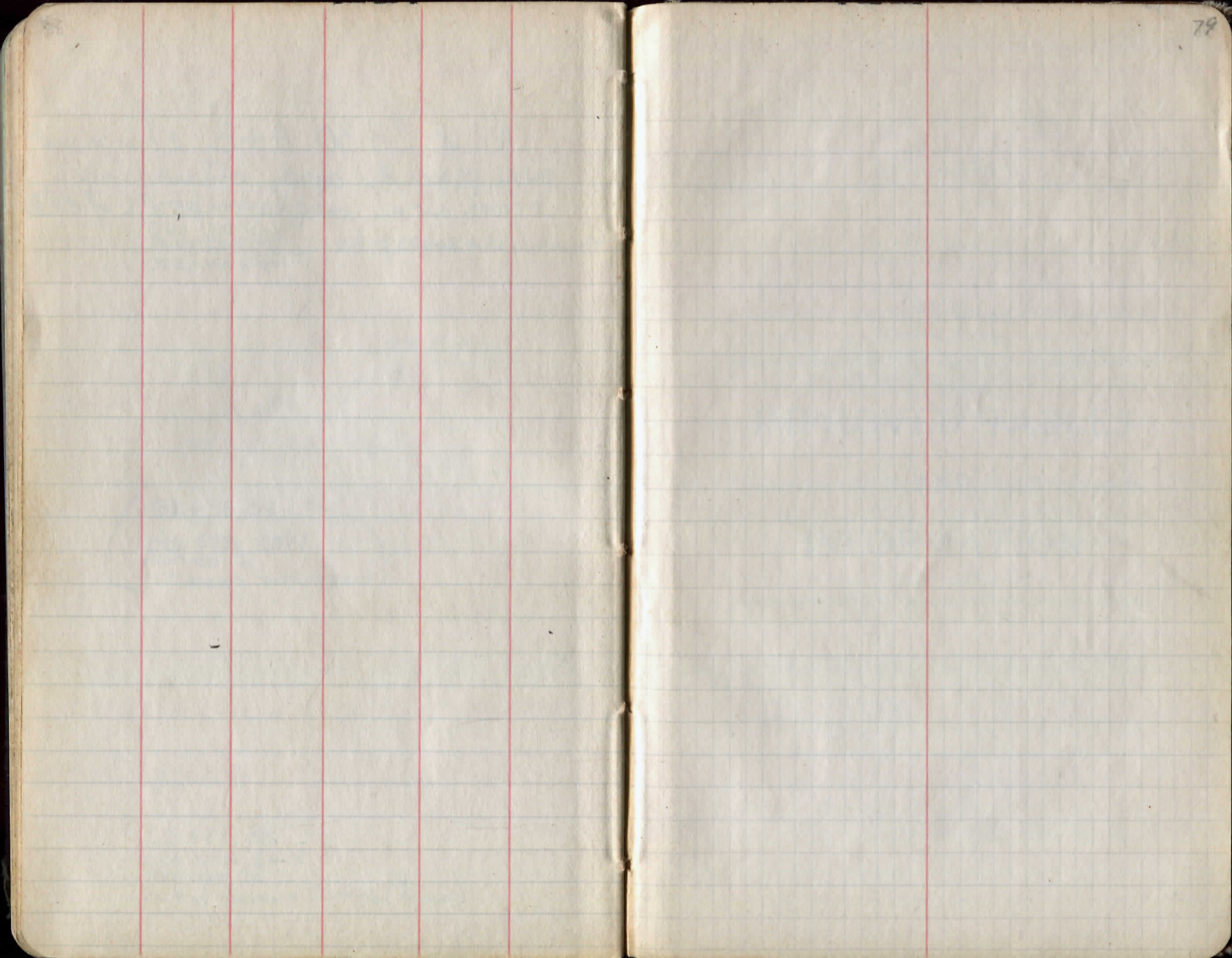
63+16<sup>+</sup>

⊗ Pekin Rd.

63+17.38

Obs STA 2014  
mon box fd  
INT of Caves + Dives (Pekin)

All of CH 30 A+B C/monument  
are placed and offset and  
errors are on plat for CL of CH 30



557

$10.11$   
 $74.15$   
 $-11.43$   


---

 $82.42$   
 $74.99$   


---

 $87.41$   


---

 $71.54$   
 $-8.87$   


---

 $3.74$   
 $77.51$   
 $-4.95$   


---

 $74.87$   
 $-5.87$   


---

 $80.74$   
 $3.95$   


---

 $76.79$

$80+69.36$   
 $28+22.55$   


---

 $52+6.81$   
 $63+59.68$   


---

 $116+66.29$

5.1

5.5

3.3

30

TABLE No. 1

83.00

7

63.19

11.6

27.81

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## IMPROVED TABLES

### AND

## INFORMATION

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## DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope  $1\frac{1}{2}$  to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

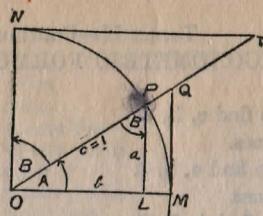


TABLE II  
TRIGONOMETRIC FORMULÆ.

$$\angle A = \angle MOP \quad \angle B = \angle PON = \angle OPL$$

$$R = OB = c = 1$$

$$\sin A = \frac{a}{c} = \frac{a}{1} = a = \cos B = LP$$

$$\cos A = \frac{b}{c} = \frac{b}{1} = b = \sin B = OL$$

$$\tan A = \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ$$

$$\cot A = \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT$$

$$\sec A = \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ$$

$$\csc A = \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT$$

$$\text{vers } A = \frac{LM}{OP} = LM = \text{covers } B \#$$

$$\text{covers } A = \frac{OP - LP}{OP} = OP - LP = \text{vers } B$$

$$\text{exsec } A = PQ = \text{coexsec } B$$

$$\text{coexsec } A = PT = \text{exsec } B$$

$$\sin \frac{1}{2} A = \sqrt{\frac{1 - \cos A}{2}} \quad \cos \frac{1}{2} A = \sqrt{\frac{1 + \cos A}{2}}$$

$$\sin 2A = 2 \sin A \cos A \quad \cos 2A = \cos^2 A - \sin^2 A$$

$$\text{Law of Lines} \quad \frac{\sin A}{a} = \frac{\sin B}{B} = \frac{\sin C}{C}$$

$$\text{Law of Cosines} \quad c^2 = a^2 + b^2 - 2ab \cos C$$

$$\text{Law of Tangents} \quad \frac{a+b}{a-b} = \frac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)}$$

TABLE II—Continued  
TRIGONOMETRIC FORMULAE (continued)

In any triangle:

Given a, b, C; to find c, B, A.

Use Law of Lines.

Given A, B, c; to find a, b, C.

Use Law of Lines.

Given a, b, c; to find A, B, C.

$$\text{Let } \frac{a+b+c}{2} = s, \sqrt{\frac{(s-a)(s-b)(s-c)}{s}} = r$$

$$\cos \frac{1}{2} A = \frac{r}{\sqrt{bc}}$$

$$\tan \frac{1}{2} A = \frac{r}{s-a}$$

$$\tan \frac{1}{2} B = \frac{r}{s-b}$$

$$\tan \frac{1}{2} C = \frac{r}{s-c}$$

Area of a triangle:

$$\text{Area} = \frac{1}{2} ab \sin C$$

$$\text{Area} = \sqrt{s(s-a)(s-b)(s-c)}$$

PRISMOIDAL FORMULA.

$$\text{Vol.} = \frac{h}{6} (B+b+4M)$$

h = altitude; b, B = bases; M = midsection

TABLE III  
INCHES AND FRACTIONS OF AN INCH IN DECIMALS OF A FOOT

	0	1	2	3	4	5	6	7	8	9	10	11
$\frac{1}{16}$	.0052	.0885	.1719	.2552	.3385	.4219	.5052	.5885	.6719	.7552	.8385	.9219
$\frac{1}{8}$	.0104	.0938	.1771	.2604	.3438	.4271	.5104	.5938	.6771	.7604	.8438	.9271
$\frac{3}{16}$	.0156	.0990	.1823	.2656	.3490	.4323	.5156	.5990	.6823	.7656	.8490	.9323
$\frac{1}{4}$	.0208	.1042	.1875	.2708	.3542	.4375	.5208	.6042	.6875	.7708	.8542	.9375
$\frac{5}{16}$	.0260	.1094	.1927	.2760	.3594	.4427	.5260	.6094	.6927	.7760	.8594	.9427
$\frac{3}{8}$	.0313	.1146	.1979	.2813	.3646	.4479	.5313	.6146	.6979	.7813	.8646	.9479
$\frac{7}{16}$	.0365	.1198	.2031	.2865	.3698	.4531	.5365	.6198	.7031	.7865	.8698	.9531
$\frac{1}{2}$	.0417	.1250	.2083	.2917	.3750	.4583	.5417	.6250	.7083	.7917	.8750	.9583
$\frac{9}{16}$	.0469	.1302	.2135	.2969	.3803	.4635	.5469	.6302	.7135	.7969	.8802	.9635
$\frac{5}{8}$	.0521	.1354	.2188	.3021	.3854	.4688	.5521	.6354	.7188	.8021	.8854	.9688
$\frac{11}{16}$	.0573	.1406	.2240	.3073	.3906	.4740	.5573	.6406	.7240	.8073	.8906	.9740
$\frac{3}{4}$	.0625	.1458	.2292	.3125	.3958	.4792	.5625	.6458	.7292	.8125	.8958	.9792
$\frac{13}{16}$	.0677	.1510	.2344	.3177	.4010	.4844	.5677	.6510	.7344	.8177	.9010	.9844
$\frac{7}{8}$	.0729	.1563	.2396	.3229	.4063	.4896	.5729	.6563	.7396	.8229	.9063	.9896
$\frac{15}{16}$	.0781	.1615	.2448	.3281	.4115	.4948	.5781	.6615	.7448	.8281	.9115	.9948
1	.0833	.1667	.2500	.3333	.4167	.5000	.5833	.6667	.7500	.8333	.9167	1.000
	0	1	2	3	4	5	6	7	8	9	10	11

TABLE IV  
USEFUL RELATIONS.

Lineal feet	×.00019	= miles
Lineal yards	×.0006	= miles
Square inches	×.007	= square feet
Square feet	×.111	= square yards
Square yards	×.0002067	= acres
Acres	×4840	= square yards
Cubic inches	×.00058	= cubic feet
Cubic feet	×.03704	= cubic yards
Links	×.22	= yards
Links	×.66	= feet
Feet	×1.5	= links

$$360^\circ = 21600' = 1296000''$$

$$\text{Radius} = \text{arc of } 57.2957790^\circ$$

$$\text{Arc of } 1^\circ (\text{radius} = 1) = .017453292$$

$$\text{Arc of } 1' (\text{radius} = 1) = .000290888$$

$$\text{Arc of } 1'' (\text{radius} = 1) = .000004848$$

$$\pi = 3.141592654 \quad \sqrt{\frac{1}{\pi}} = 0.564190$$

$$\frac{\pi}{4} = 0.785398163 \quad \sqrt[2]{\frac{6}{\pi}} = 1.240700982$$

$$\frac{\pi}{6} = 0.523598776 \quad \pi^2 = 9.869604401$$

$$\sqrt{\frac{4}{\pi}} = 1.128379167 \quad \frac{1}{\pi^2} = 0.101321184$$

$$\frac{\pi}{6} = 0.523598776 \quad \sqrt{\pi} = 1.772453851$$

$$\frac{4\pi}{3} = 4.188790205 \quad \frac{1}{\pi} = 0.3183099$$

Curvature of Earth's surface = about 0.7 feet in 1 mile

Curvature in feet = 0.667 (Dist. in miles)<sup>2</sup>

Difference between arc and chord length, 0.05 feet in 11½ miles

$$\text{Probable error of a single observation} = 0.6754 \sqrt{\frac{M V^2}{n-1}}$$

Error in chaining of 0.01 feet in 100 feet:

Due to—

1. Length of tape error of 0.01 feet
2. Alignment. One end 1.4 feet out of line
3. Sag of tape at centre of 0.61 feet.
4. Temperature difference of 15°
5. Difference of pull of 15 lbs.

STADIA REDUCTION FORMULAE.

Horizontal Distance = R — R sin<sup>2</sup> a + C cos a

Vertical Distance = R ½ sin 2 a + C sin a

$$R = \text{Reading} \times \frac{\text{distance from Object glass to cross hairs}}{\text{distance between cross hairs}}$$

C = distance from Object glass to cross hairs + distance from Object glass to center of instrument.

a = angle of elevation for mid Reading



TABLE VI (continued)  
SINES, COSINES, TANGENTS, COTANGENTS (continued)

deg	sin 0'	tan 0'	sin 10'	tan 10'	sin 20'	tan 20'	sin 30'	tan 30'	sin 40'	tan 40'	sin 50'	tan 50'	deg
46	7193	1.0355	7214	1.0416	7234	1.0477	7254	1.0533	7274	1.0599	7294	1.0661	43
47	314	.0724	333	.0786	353	.0850	373	.0913	392	.0977	412	1.041	42
48	431	.1106	451	.1171	470	.1237	490	.1303	509	.1369	528	1.436	41
49	547	.1504	566	.1571	585	.1640	604	.1708	623	.1778	642	1.847	40
50	660	1.1918	7679	1.1988	7698	1.2059	7716	1.2131	7735	.2647	7753	1.2276	39
51	771	.2349	790	.2423	808	.2497	826	.2572	844	.3111	862	.2723	38
52	880	.2799	898	.2876	916	.2954	934	.3032	951	.3597	969	.3190	37
53	986	.3270	8004	.3351	8021	.3452	8039	.3514	8056	.4106	8073	.3680	36
54	8090	.3764	107	.3848	124	.3934	141	.4019	158	.4641	175	.4193	35
55	192	.4281	208	.4370	225	.4460	241	.4550	258	.5204	274	.4733	34
56	290	.4826	307	.4919	323	.5013	339	.5108	355	.5798	371	.5301	33
57	387	.5399	403	.5497	418	.5597	434	.5697	450	.6426	465	.5900	32
58	480	.6003	496	.6107	511	.6212	526	.6319	542	.7090	557	.6534	31
59	572	.6643	587	.6753	601	.6864	616	.6977	631	.646	646	.7205	30
60	660	1.7321	8675	1.7437	8689	1.7556	8704	1.7675	8718	1.7797	8732	1.7917	29
61	746	.8040	760	.8165	774	.8291	788	.8418	802	.8546	816	.8676	28
62	829	.8807	843	.8940	857	.9074	870	.9210	884	.9347	897	.9486	27
63	910	.9626	923	.9768	936	.9912	949	2.0057	962	2.0204	975	2.0353	26
64	988	2.0503	9001	2.0655	9013	2.0809	9026	.0965	9038	.1123	9051	1.283	25
65	9063	1.445	075	.1609	088	.1775	100	.1943	112	.2113	124	.2286	24
66	135	.2460	147	.2637	159	.2817	171	.2998	182	.3183	194	.3369	23
67	205	.3559	216	.3750	228	.3945	239	.4142	250	.4342	261	.4545	22
68	272	.4751	283	.4960	293	.5172	304	.5386	315	.5605	325	.5826	21
69	336	.6051	346	.6279	356	.6511	367	.6746	377	.6985	387	.7228	20
70	397	2.7475	9407	2.7725	9417	2.7980	9426	2.8239	9436	2.8502	9446	2.8770	19
71	455	.9042	465	.9319	474	.9600	483	.9887	492	3.0178	502	3.0475	18
72	511	3.0777	520	3.1084	528	3.1397	537	3.1716	546	.2041	555	.2371	17
73	563	.2709	572	.3052	580	.3402	588	.3759	596	.4124	605	.4495	16
74	613	.4874	621	.5261	628	.5656	636	.6059	644	.6470	652	.6891	15
75	659	.7321	667	.7760	674	.8208	681	.8657	689	.9136	696	.9617	14
76	703	4.0108	710	4.0611	717	4.1126	724	4.1653	730	4.2193	737	4.2747	13
77	744	.3315	750	.3897	757	.4494	763	.5107	769	.5736	775	.6382	12
78	781	.7046	787	.7729	793	.8439	799	.9152	805	.9894	811	5.0658	11
79	816	.1446	822	5.2257	827	5.3093	833	5.3955	838	5.4845	843	.5764	10
80	9848	5.6713	9853	5.7694	9858	5.8708	9863	5.9758	9868	6.0844	9872	6.1970	9
81	877	6.3138	881	6.4348	886	6.5606	890	6.6912	894	.8269	899	.9682	8
82	903	7.1154	907	7.2687	911	7.4287	914	7.5958	918	7.7704	922	7.9530	7
83	925	8.1443	929	8.3450	932	8.5555	936	8.7769	939	9.0098	942	9.2553	6
84	945	9.5144	948	9.7882	951	10.078	954	10.385	957	10.711	959	11.059	5
85	962	11.430	964	11.826	967	12.250	969	12.706	971	13.197	974	13.727	4
86	976	14.300	978	14.924	980	15.605	981	16.350	983	17.169	985	18.075	3
87	986	19.081	988	20.206	989	21.470	990	22.903	992	24.542	993	26.432	2
88	994	28.636	995	31.242	996	34.368	997	38.189	997	42.964	998	49.104	1
89	9998	57.290	9999	63.750	9999	85.940	9999	114.58	1.000	171.88	1.000	343.77	0
90	60'	60'	50'	50'	40'	40'	30'	30'	20'	30'	10'	10'	deg
90	cos	cot	cos	cot	cos	cot	cos	cot	cos	cot	cos	cot	deg

TABLE VII  
RODS IN FEET AND INCHES

Rods	Feet Inches	Rods	Feet Inches	Rods	Feet Inches	Rods	Feet Inches	Rods	Feet Inches
1	16-6	21	346-6	41	676-6	61	1006-6	81	1336-6
2	33-0	22	363-0	42	693-0	62	1023-0	82	1353-0
3	49-6	23	379-6	43	709-6	63	1039-6	83	1369-6
4	66-0	24	396-0	44	726-0	64	1056-0	84	1386-0
5	82-6	25	412-6	45	742-6	65	1072-6	85	1402-6
6	99-0	26	429-0	46	759-0	66	1089-0	86	1419-0
7	115-6	27	445-6	47	775-6	67	1105-6	87	1435-6
8	132-0	28	462-0	48	792-0	68	1122-0	88	1452-0
9	148-6	29	478-6	49	808-6	69	1138-6	89	1468-6
10	165-0	30	495-0	50	825-0	70	1155-0	90	1485-0
11	181-6	31	511-6	51	841-6	71	1171-6	91	1501-6
12	198-0	32	528-0	52	858-0	72	1188-0	92	1518-0
13	214-6	33	544-6	53	874-6	73	1204-6	93	1534-6
14	231-0	34	561-0	54	891-0	74	1221-0	94	1551-0
15	247-6	35	577-6	55	907-6	75	1237-6	95	1567-6
16	264-0	36	594-0	56	924-0	76	1254-0	96	1584-0
17	280-6	37	610-6	57	940-6	77	1270-6	97	1600-6
18	297-0	38	627-0	58	957-0	78	1287-0	98	1617-0
19	313-6	39	643-6	59	973-6	79	1303-6	99	1633-6
20	330-0	40	660-0	60	990-0	80	1320-0	100	1650-0

TABLE VIII  
LINKS IN FEET AND INCHES

Links	Feet Inches	Links	Feet Inches	Links	Feet Inches	Links	Feet Inches	Links	Feet Inches	Links	Feet Inches
1	0-7.92	18	11-10.56	35	23-1.20	52	34-3.84	69	45-6.48	86	56-9.12
2	1-3.84	19	12-6.48	36	23-9.12	53	34-11.76	70	46-2.40	87	57-5.04
3	1-11.76	20	13-2.40	37	24-5.04	54	35-7.68	71	46-10.32	88	58-0.96
4	2-7.68	21	13-10.32	38	25-0.96	55	36-3.60	72	47-6.24	89	58-8.88
5	3-3.60	22	14-6.24	39	25-8.88	56	36-11.52	73	48-2.16	90	59-4.80
6	3-11.52	23	15-2.16	40	26-4.80	57	37-7.44	74	48-10.08	91	60-0.72
7	4-7.44	24	15-10.08	41	27-0.72	58	38-3.36	75	49-6.00	92	60-8.64
8	5-3.36	25	16-6.00	42	27-8.64	59	38-11.28	76	50-1.92	93	61-4.56
9	5-11.28	26	17-1.92	43	28-4.56	60	39-7.20	77	50-9.84	94	62-0.48
10	6-7.20	27	17-9.84	44	29-0.48	61	40-3.12	78	51-5.76	95	62-8.40
11	7-3.12	28	18-5.76	45	29-8.40	62	40-11.04	79	52-1.68	96	63-4.32
12	7-11.04	29	19-1.68	46	30-4.32	63	41-6.96	80	52-9.60	97	64-0.24
13	8-6.96	30	19-9.60	47	31-0.24	64	42-2.88	81	53-5.52	98	64-8.16
14	9-2.88	31	20-5.52	48	31-8.16	65	42-10.80	82	54-1.44	99	65-4.08
15	9-10.80	32	21-1.44	49	32-4.08	66	43-6.72	83	54-9.36	100	66-0.00
16	10-6.72	33	21-9.36	50	33-0.00	67	44-2.64	84	55-5.28	101	66-7.92
17	11-2.64	34	22-5.28	51	33-7.92	68	44-10.56	85	56-1.20	102	67-3.84

TABLE IX. TANGENTS AND EXTERNALS TO A 1° CURVE

I	T	E	I=10°	I	T	E	I=20°	I	T	E	I=30°
1°	50.00	.218	+	11°	551.70	26.500	+	21°	1061.9	97.577	+
10'	58.34	.297		10'	560.11	27.313		10'	1070.6	99.155	
20'	66.67	.388	5° C.	20'	568.53	28.137	5° C.	20'	1079.2	100.75	5° C.
30'	75.01	.491	T	30'	576.95	28.974	T	30'	1087.8	102.35	T
40'	83.34	.606	.03	40'	585.36	29.824	.06	40'	1096.4	103.97	.10
50'	91.68	.733	E	50'	593.79	30.686	E	50'	1105.1	105.60	E
2°	100.01	.873	.001	12°	602.21	31.561	.006	22°	1113.7	107.24	.013
10'	108.35	1.024		10'	610.64	32.447		10'	1122.4	108.90	
20'	116.68	1.188		20'	619.07	33.347		20'	1131.0	110.57	
30'	125.02	1.364		30'	627.50	34.259		30'	1139.7	112.25	
40'	133.36	1.552		40'	635.93	35.183		40'	1148.4	113.95	
50'	141.70	1.752		50'	644.37	36.120		50'	1157.0	115.66	
3°	150.04	1.964	10° C.	13°	652.81	37.070	10° C.	23°	1165.7	117.38	10° C.
10'	158.38	2.188	T	10'	661.25	38.031	T	10'	1174.4	119.12	T
20'	166.72	2.425	.06	20'	669.70	39.006	.13	20'	1183.1	120.87	.19
30'	175.06	2.674	E	30'	678.15	39.993	E	30'	1191.8	122.63	E
40'	183.40	2.934	.003	40'	686.60	40.992	.011	40'	1200.5	124.41	.025
50'	191.74	3.207		50'	695.06	42.004		50'	1209.2	126.20	
4°	200.08	3.492		14°	703.51	43.029		24°	1217.9	128.00	
10'	208.43	3.790		10'	711.97	44.066		10'	1226.6	129.82	
20'	216.77	4.099		20'	720.44	45.116		20'	1235.3	131.65	
30'	225.12	4.421		30'	728.90	46.178		30'	1244.0	133.50	
40'	233.47	4.755		40'	737.37	47.253		40'	1252.8	135.35	
50'	241.81	5.100	15° C.	50'	745.85	48.341	15° C.	50'	1261.5	137.23	15° C.
5°	250.16	5.459	T	15°	754.32	49.441	T	25°	1270.2	139.11	T
10'	258.51	5.829	.09	10'	762.80	50.554	.19	10'	1279.0	141.01	.29
20'	266.86	6.211	E	20'	771.29	51.679	E	20'	1287.7	142.93	E
30'	275.21	6.606	.004	30'	779.77	52.818	.017	30'	1296.5	144.85	.033
40'	283.57	7.013		40'	788.26	53.969		40'	1305.3	146.79	
50'	291.92	7.432		50'	796.75	55.132		50'	1314.0	148.75	
6°	300.28	7.863		16°	805.25	56.309		26°	1322.8	150.71	
10'	308.64	8.307		10'	813.75	57.498		10'	1331.6	152.69	
20'	316.99	8.762		20'	822.25	58.699		20'	1340.4	154.69	
30'	325.35	9.230		30'	830.76	59.914		30'	1349.2	156.70	
40'	333.71	9.710	20° C.	40'	839.27	61.141	20° C.	40'	1358.0	158.72	20° C.
50'	342.08	10.202	T	50'	847.78	62.381	T	50'	1366.8	160.76	T
7°	350.44	10.707	.13	17°	856.30	63.634	.26	27°	1375.6	162.81	.39
10'	358.81	11.224	E	10'	864.82	64.900	E	10'	1384.4	164.86	E
20'	367.17	11.753	.006	20'	873.35	66.178	.022	20'	1393.2	166.95	.051
30'	375.54	12.294		30'	881.88	67.470		30'	1402.0	169.04	
40'	383.91	12.847		40'	890.41	68.774		40'	1410.9	171.15	
50'	392.28	13.413		50'	898.95	70.091		50'	1419.7	173.27	
8°	400.66	13.991		18°	907.49	71.421		28°	1428.6	175.41	
10'	409.03	14.582		10'	916.03	72.764		10'	1437.4	177.55	
20'	417.41	15.184	25° C.	20'	924.58	74.119	25° C.	20'	1446.3	179.72	25° C.
30'	425.79	15.799	T	30'	933.13	75.488	T	30'	1455.1	181.89	T
40'	434.17	16.426	.16	40'	941.69	76.869	.32	40'	1464.0	184.08	.49
50'	442.55	17.065	E	50'	950.25	78.264	E	50'	1472.9	186.29	E
9°	450.93	17.717	.007	19°	958.81	79.671	.028	29°	1481.8	188.51	.065
10'	459.32	18.381		10'	967.38	81.092		10'	1490.7	190.74	
20'	467.71	19.058		20'	975.96	82.525		20'	1499.6	192.99	
30'	476.10	19.746		30'	984.53	83.972		30'	1508.5	195.25	
40'	484.49	20.447		40'	993.12	85.431		40'	1517.4	197.53	
50'	492.88	21.161		50'	1001.7	86.904		50'	1526.3	199.82	
10°	501.28	21.887	30° C.	20°	1010.3	88.389	30° C.	30°	1535.3	202.12	30° C.
10'	509.68	22.624	T	10'	1018.9	89.888	T	10'	1544.2	204.44	T
20'	518.08	23.375	.19	20'	1027.5	91.399	.39	20'	1553.1	206.77	.59
30'	526.48	24.138	E	30'	1036.1	92.924	E	30'	1562.1	209.12	E
40'	534.89	24.913		40'	1044.7	94.462		40'	1571.0	211.48	
50'	543.29	25.700	.008	50'	1053.3	96.013	.034	50'	1580.0	213.86	.078

T = R tan 1/2 I

E = R exsec 1/2 I

TABLE IX. TANGENTS AND EXTERNALS TO A 1° CURVE

I	T	E	I=40°	I	T	E	I=50°	I	T	E	I=60°
31°	1589.0	216.3	+	41°	2142.2	387.4	+	51°	2732.9	618.4	+
10'	1598.0	218.7		10'	2151.7	390.7		10'	2743.1	622.8	
20'	1606.9	221.1	5° C.	20'	2161.2	394.1	5° C.	20'	2753.4	627.2	5° C.
30'	1615.9	223.5	T	30'	2170.8	397.4	T	30'	2763.7	631.7	T
40'	1624.9	226.0	.13	40'	2180.3	400.8	.17	40'	2773.9	636.2	.21
50'	1633.9	228.4	E	50'	2189.9	404.2	E	50'	2784.2	640.7	E
32°	1643.0	230.9	.023	42°	2199.4	407.6	.037	52°	2794.5	645.2	.056
10'	1652.0	233.4		10'	2209.0	411.1		10'	2804.9	649.7	
20'	1661.0	235.9		20'	2218.6	414.5		20'	2815.2	654.3	
30'	1670.0	238.4		30'	2228.1	418.0		30'	2825.6	658.8	
40'	1679.1	241.0		40'	2237.7	421.4		40'	2835.9	663.4	
50'	1688.1	243.5		50'	2247.3	425.0		50'	2846.3	668.0	
33°	1697.2	246.1	10° C.	43°	2257.0	428.5	10° C.	53°	2856.7	672.7	10° C.
10'	1706.3	248.7	T	10'	2266.6	432.0	T	10'	2867.1	677.3	T
20'	1715.3	251.3	.13	20'	2276.2	435.6	.34	20'	2877.5	682.0	.42
30'	1724.4	253.9	.26	30'	2285.9	439.2	E	30'	2888.0	686.7	E
40'	1733.5	256.5	E	40'	2295.6	442.8	E	40'	2898.4	691.4	E
50'	1742.6	259.1	.046	50'	2305.2	446.4	.075	50'	2908.9	696.1	.112
34°	1751.7	261.8		44°	2314.9	450.0		54°	2919.4	700.9	
10'	1760.8	264.5		10'	2324.6	453.6		10'	2929.9	705.7	
20'	1770.0	267.2		20'	2334.3	457.3		20'	2940.4	710.5	
30'	1779.1	269.9		30'	2344.1	461.0		30'	2951.0	715.3	
40'	1788.2	272.6		40'	2353.8	464.6		40'	2961.5	720.1	
50'	1797.4	275.3	15° C.	50'	2363.5	468.4	15° C.	50'	2972.1	725.0	15° C.
35°	1806.6	278.1	T	45°	2373.3	472.1	T	55°	2982.7	729.9	T
10'	1815.7	280.8	.40	10'	2383.1	475.8	.51	10'	2993.3	734.8	.63
20'	1824.9	283.6	E	20'	2392.8	479.6	E	20'	3003.9	739.7	E
30'	1834.1	286.4	.070	30'	2402.6	483.4	.116	30'	3014.5	744.6	.168
40'	1843.3	289.2		40'	2412.4	487.2		40'	3025.2	749.6	
50'	1852.5	292.0		50'	2422.3	491.0		50'	3035.8	754.6	
36°	1861.7	294.9		46°	2432.1	494.8		56°	3046.5	759.6	
10'	1870.9	297.7		10'	2441.9	498.7		10'	3057.2	764.6	
20'	1880.1	300.6		20'	2451.8	502.5		20'	3067.9	769.7	
30'	1889.4	303.5		30'	2461.7	506.4		30'	3078.7	774.7	
40'	1898.6	306.4	20° C.	40'	2471.5	510.3	20° C.	40'	3089.4	779.8	20° C.
50'	1907.9	309.3	T	50'	2481.4	514.3	T	50'	3100.2	784.9	T
37°	1917.1	312.2	.53	47°	2491.3	518.2	.68	57°	3110.9	790.1	.84
10'	1926.4	315.2	E	10'	2501.2	522.2	E	10'	3121.7	795.2	E
20'	1935.7	318.1	.093	20'	2511.2	526.1	.151	20'	3132.6	800.4	.225
30'	1945.0	321.1		30'	2521.1	530.1		30'	3143.4	805.6	
40'	1954.3	324.1		40'	2531.1	534.2		40'	3154.2	810.9	
50'	1963.6	327.1		50'	2541.0	538.2		50'	3165.1	816.1	
38°	1972.9	330.2		48°	2551.0	542.2		58°	3176.0	821.4	
10'	1982.2	333.2	25° C.	10'	2561.0	546.3	25° C.	10'	3186.9	826.7	25° C.
20'	1991.5	336.3	T	20'	2571.0	550.4	T	20'	3197.8	832.0	T
30'	2000.9	339.3	.67	30'	2581.0	554.5	.85	30'	3208.8	837.3	.85
40'	2010.2	342.4	E	40'	2591.0	558.6	E	40'	3219.7	842.7	E
50'	2019.6	345.5	.117	50'	2601.1	562.8	.189	50'	3230.7	848.1	.105
39°	2029.0	348.6		49°	2611.2						

TABLE IX. TANGENTS AND EXTERNALS TO A 1° CURVE

I	T	E	I=70°	I	T	E	I=80°	I	T	E	I=90°						
61°	3375.0	920.2	+	71°	4086.9	1308.2	+	81°	4893.6	1805.3	+						
10'	3386.3	925.9		5° C.	10'	4099.5		1315.6	5° C.	10'		4908.0	1814.7	5° C.			
20'	3397.5	931.6			20'	4112.1		1322.9		20'		4922.5	1824.1		20'	4956.8	1833.6
30'	3408.8	937.3			T	4124.8		1330.3		T		4937.0	1833.6		T	4961.1	1843.1
40'	3420.1	943.1			.25	4137.4		1337.7		.30		4947.5	1843.1		.36	4976.1	1852.6
50'	3431.4	948.9	E	4150.1	1345.1	E	4958.0	1852.6	E	4986.1	1862.2						
62°	3442.7	954.8	.080	72°	4162.8	1352.6	.110	82°	4980.7	1862.2	.149						
10'	3454.1	960.6		10'	4175.6	1360.1		10'	4995.4	1871.8		10'	5010.0	1881.5			
20'	3465.4	966.5		20'	4188.5	1367.6		20'	5010.0	1881.5		20'	5024.8	1891.2			
30'	3476.8	972.4		30'	4201.2	1375.2		30'	5024.8	1891.2		30'	5039.5	1900.9			
40'	3488.3	978.3		40'	4214.0	1382.8		40'	5039.5	1900.9		40'	5054.3	1910.7			
50'	3499.7	984.3	E	4226.8	1390.4	E	5054.3	1910.7	E	5069.2	1920.5						
63°	3511.1	990.2	10° C.	73°	4239.7	1398.0	10° C.	83°	5069.2	1920.5	10° C.						
10'	3522.6	996.2		T	4252.6	1405.7		T	5084.0	1930.4		T	5098.9	1940.3			
20'	3534.1	1002.3		.51	4265.6	1413.5		.61	5103.9	1950.3		.72	5113.9	1960.2			
30'	3545.6	1008.3		E	4278.5	1421.2		E	5128.9	1960.2		E	5143.9	1970.3			
40'	3557.2	1014.4		.159	4291.5	1429.0		.220	5143.9	1970.3		.299	5159.0	1980.4			
50'	3568.7	1020.5	E	4304.6	1436.8	E	5174.1	1990.5	E	5189.3	2000.6						
64°	3580.3	1026.6	15° C.	74°	4317.6	1444.6	15° C.	84°	5174.1	1990.5	15° C.						
10'	3591.9	1032.8		10'	4330.7	1452.5		10'	5189.3	2000.6		10'	5204.4	2010.8			
20'	3603.5	1039.0		20'	4343.8	1460.4		20'	5204.4	2010.8		20'	5219.7	2021.1			
30'	3615.1	1045.2		30'	4356.9	1468.4		30'	5219.7	2021.1		30'	5234.6	2031.4			
40'	3626.8	1051.4		40'	4370.1	1476.4		40'	5234.6	2031.4		40'	5250.3	2041.7			
50'	3638.5	1057.7	E	4383.3	1484.4	E	5250.3	2041.7	E	5265.6	2052.1						
65°	3650.2	1063.9	T	75°	4396.5	1492.4	T	85°	5250.3	2041.7	T						
10'	3661.9	1070.2		.76	4409.8	1500.5		.91	5265.6	2052.1		1.09	5281.0	2062.5			
20'	3673.7	1076.6		E	4423.1	1508.6		E	5296.4	2073.0		E	5311.9	2083.5			
30'	3685.4	1082.9		.240	4436.4	1516.7		.332	5311.9	2083.5		.450	5327.4	2094.1			
40'	3697.2	1089.3		40'	4449.7	1524.9		40'	5327.4	2094.1		40'	5343.2	2104.7			
50'	3709.0	1095.7	E	4463.1	1533.1	E	5343.2	2104.7	E	5358.6	2115.3						
66°	3720.9	1102.2	20° C.	76°	4476.5	1541.4	20° C.	86°	5343.2	2104.7	20° C.						
10'	3732.7	1108.6		10'	4489.9	1549.7		10'	5358.6	2115.3		10'	5374.2	2126.0			
20'	3744.6	1115.1		20'	4503.3	1558.0		20'	5374.2	2126.0		20'	5389.9	2136.7			
30'	3756.5	1121.7		30'	4516.9	1566.3		30'	5405.6	2147.5		30'	5421.4	2158.4			
40'	3768.5	1128.2		40'	4530.4	1574.7		40'	5421.4	2158.4		40'	5437.2	2169.2			
50'	3780.4	1134.8	E	4544.0	1583.1	E	5437.2	2169.2	E	5453.1	2180.2						
67°	3792.4	1141.4	1.02	77°	4557.6	1591.6	1.22	87°	5437.2	2169.2	1.45						
10'	3804.4	1148.0		E	4571.2	1600.1		E	5453.1	2180.2		E	5469.0	2191.1			
20'	3816.4	1154.7		.321	4584.8	1608.6		.445	5469.0	2191.1		.603	5484.9	2202.2			
30'	3828.4	1161.3		30'	4598.5	1617.1		30'	5484.9	2202.2		30'	5500.9	2213.2			
40'	3840.5	1168.1		40'	4612.2	1625.7		40'	5500.9	2213.2		40'	5517.0	2224.3			
50'	3852.6	1174.8	E	4626.0	1634.4	E	5517.0	2224.3	E	5533.1	2235.5						
68°	3864.7	1181.6	25° C.	78°	4639.8	1643.0	25° C.	88°	5533.1	2235.5	25° C.						
10'	3876.8	1188.4		10'	4653.6	1651.7		10'	5549.2	2246.7		10'	5565.4	2258.0			
20'	3889.0	1195.2		20'	4667.4	1660.5		20'	5565.4	2258.0		20'	5581.6	2269.3			
30'	3901.2	1202.0		T	4681.3	1669.2		T	5581.6	2269.3		T	5597.8	2280.6			
40'	3913.4	1208.9		1.28	4695.2	1678.1		1.53	5597.8	2280.6		1.83	5614.2	2292.0			
50'	3925.6	1215.8	E	4709.2	1686.9	E	5614.2	2292.0	E	5630.5	2303.5						
69°	3937.9	1222.7	.403	79°	4723.2	1695.8	.558	89°	5630.5	2303.5	.756						
10'	3950.2	1229.7		10'	4737.2	1704.7		10'	5646.9	2315.0		10'	5663.4	2326.6			
20'	3962.5	1236.7		20'	4751.2	1713.7		20'	5663.4	2326.6		20'	5679.9	2338.2			
30'	3974.8	1243.7		30'	4765.3	1722.7		30'	5679.9	2338.2		30'	5696.4	2349.8			
40'	3987.2	1250.8		40'	4779.4	1731.7		40'	5696.4	2349.8		40'	5713.0	2361.5			
50'	3999.5	1257.9	E	4793.6	1740.8	E	5713.0	2361.5	E	5729.7	2373.3						
70°	4011.9	1265.0	30° C.	80°	4807.7	1749.9	30° C.	90°	5729.7	2373.3	30° C.						
10'	4024.4	1272.1		T	4822.0	1759.0		T	5746.3	2385.1		T	5763.3	2397.0			
20'	4036.8	1279.3		1.54	4836.2	1768.2		1.84	5763.3	2397.0		2.20	5779.9	2408.9			
30'	4049.3	1286.5		E	4850.5	1777.4		E	5796.7	2420.9		E	5813.6	2432.9			
40'	4061.8	1293.6		.485	4864.8	1786.7		.671	5813.6	2432.9		.910	5830.5	2447.0			
50'	4074.4	1300.9	E	4879.2	1796.0	E	5830.5	2447.0	E	5848.0	2461.3						

T = R tan 1/2 I

E = R exsec 1/2 I

TABLE IX. TANGENTS AND EXTERNALS TO A 1° CURVE

I	T	E	I=100°	I	T	E	I=110°	I	T	E	I=120°						
91°	5830.5	2444.9	+	101°	6950.6	3278.1	+	111°	8336.7	4386.1	+						
10'	5847.5	2457.1		5° C.	10'	6971.3		3294.1	5° C.	10'		8362.7	4407.6	5° C.			
20'	5864.6	2469.3			20'	6992.0		3310.1		20'		8388.9	4429.2		20'	8415.1	4450.9
30'	5881.7	2481.5			T	7012.7		3326.1		T		8415.1	4450.9		T	8441.5	4472.7
40'	5898.8	2493.8			.43	7033.6		3342.3		.51		8441.5	4472.7		.62	8468.0	4494.6
50'	5916.0	2506.1	E	7054.5	3358.5	E	8468.0	4494.6	E	8494.6	4516.6						
92°	5933.2	2518.5	.200	102°	7075.5	3374.9	.268	112°	8494.6	4516.6	.360						
10'	5950.5	2531.0		10'	7096.6	3391.2		10'	8521.3	4538.8		10'	8548.1	4561.1			
20'	5967.9	2543.5		20'	7117.8	3407.7		20'	8548.1	4561.1		20'	8575.0	4583.4			
30'	5985.3	2556.0		30'	7139.0	3424.3		30'	8575.0	4583.4		30'	8602.1	4606.0			
40'	6002.7	2568.6		40'	7160.3	3440.9		40'	8602.1	4606.0		40'	8629.3	4628.6			
50'	6020.2	2581.3	E	7181.7	3457.6	E	8629.3	4628.6	E	8656.6	4651.3						
93°	6037.8	2594.0	10° C.	103°	7203.2	3474.4	10° C.	113°	8656.6	4651.3	10° C.						
10'	6055.4	2606.8		T	7224.7	3491.3		T	8684.0	4674.2		T	8711.5	4697.2			
20'	6073.1	2619.7		.86	7246.3	3508.2		.103	8711.5	4697.2		.125	8739.2	4720.3			
30'	6090.8	2632.6		E	7268.0	3525.2		E	8739.2	4720.3		E	8767.0	4743.6			
40'	6108.6	2645.5		.401	7289.8	3542.4		.536	8767.0	4743.6		.721	8794.9	4766.9			
50'	6126.4	2658.5	E	7311.7	3559.6	E	8794.9	4766.9	E	8822.9	4790.4						
94°	6144.3	2671.6	15° C.	104°	7333.6	3576.8	15° C.	114°	8822.9	4790.4	15° C.						
10'	6162.2	2684.7		10'	7355.6	3594.2		10'	8851.0	4814.1		10'	8879.3	4837.8			
20'	6180.2	2697.9		20'	7377.8	3611.7		20'	8879.3	4837.8		20'	8907.7	4861.7			
30'	6198.3	2711.2		30'	7399.9	3629.2		30'	8907.7	4861.7		30'	8936.3	4885.7			
40'	6216.4	2724.5		40'	7422.2	3646.8		40'	8936.3	4885.7		40'	8965.0	4909.9			
50'	6234.6	2737.9	E	7444.6	3664.5	E	8965.0	4909.9	E	8993.8	4934.1						
95°	6252.8	2751.3	T	105°	7467.0	3682.3	T	115°	8993.8	4934.1	T						
10'	6271.1	2764.8		1.30	7489.6	3700.2		1.56	9022.7	4958.6		1.93	9051.7	4983.1			
20'	6289.4	2778.3		E	7512.2	3718.2		E	9051.7	4983.1		E	9080.9	5007.8			
30'	6307.9	2792.0		.604	7534.9	3736.2		.806	9080.9	5007.8		1.09	9110.3	5032.6			
40'	6326.3	2805.6		40'	7557.7	3754.4		50'	9110.3	5032.6		50'	9139.8	5057.6			
50'	6344.8	2819.4	E	7580.5	3772.6	E	9139.8	5057.6	E	9169.4	5082.7						
96°	6363.4	2833.2	106°	106°	7603.5	3791.0	106°	116°	9169.4	5082.7	106°						
10'	6382.1	2847.0		10'	7626.6	3809.4		10'	9199.1	5107.9		10'	9229.0	5133.3			
20'	6400.8	2861.0		20'	7649.7	3827.9		20'	9229.0	5133.3		20'	9259.5	5158.8			
30'	6419.5	2875.0		30'	7672.9	3846.5		30'	9259.5	5158.8		30'	9290.2	5184.5			
40'	6438.4	2889.0		40'	7696.3	3865.2		40'	9290.2	5184.5		40'	9319.5	5210.3			
50'	6457.3	2903.1	T	7719.7	3884.0	T	9319.5	5210.3	T	9349.9	5236.2						
97°	6476.2	2917.3	1.74	107°	7743.2	3902.9	1.08	117°	9349.9	5236.2	1.46						
10'	6495.2	2931.6		E	7766.8	3921.9		E	9380.5	5262.3							

TABLE X.  
MIDDLE ORDINATES OF RAILS  
Length of Rail (feet)

C o /	R Feet	30 Inch	28 Inch	26 Inch	24 Inch	22 Inch	20 Inch	C o	R Feet	30 Inch	28 Inch	26 Inch	24 Inch	22 Inch	20 Inch
0-20	17189	.08	.07	.06	.05	.04	.03	8	716.8	1.88	1.64	1.42	1.20	1.01	.84
0-40	8594	.16	.14	.12	.10	.08	.07	9	637.3	2.12	1.84	1.60	1.35	1.14	.94
1-0	5730	.24	.20	.18	.15	.13	.10	10	573.7	2.36	2.05	1.78	1.50	1.27	1.04
1-20	4297	.31	.27	.23	.20	.17	.13	11	521.7	2.59	2.26	1.95	1.65	1.39	1.15
1-40	3438	.39	.34	.29	.25	.21	.17	12	478.3	3.83	2.47	2.15	1.81	1.54	1.26
2-0	2865	.47	.41	.35	.30	.25	.20	13	441.7	3.05	2.66	2.30	1.96	1.66	1.36
2-20	2456	.55	.48	.41	.35	.29	.23	14	410.3	3.30	2.87	2.48	2.10	1.78	1.46
2-40	2149	.63	.55	.47	.40	.33	.27	15	383.1	3.54	3.08	2.68	2.26	1.91	1.57
3-0	1910	.71	.62	.53	.45	.38	.31	16	359.3	3.76	3.28	2.83	2.40	2.04	1.67
3-20	1719	.78	.68	.59	.50	.42	.35	17	338.3	4.00	3.48	3.02	2.57	2.16	1.78
3-40	1563	.86	.75	.65	.55	.46	.38	18	319.6	4.21	3.67	3.18	2.70	2.28	1.87
4-0	1433	.94	.82	.71	.60	.50	.42	19	302.9	4.45	3.89	3.36	2.86	2.41	1.98
4-20	1323	1.02	.89	.77	.65	.55	.45	20	287.9	4.70	4.09	3.55	3.00	2.54	2.09
4-40	1228	1.10	.96	.83	.70	.59	.48	22	262.0	5.16	4.44	3.84	3.30	2.80	2.29
5	1146	1.18	1.03	.89	.75	.63	.52	24	240.5	5.64	4.92	4.20	3.59	3.04	2.50
6	955.3	1.41	1.23	1.06	.90	.76	.62	26	222.3	6.07	5.29	4.58	3.88	3.29	2.70
7	819.0	1.65	1.44	1.24	1.05	.89	.73								

TABLE XI.  
SHORT RADIUS CURVES

Radius Feet	Chord Feet	Central Angle	Deflection Angle	Deflection for 1 Foot
35	10	16-26	8-13	49.3
45	10	12-46	6-23	38.3
50	15	17-16	8-38	34.5
60	15	14-22	7-11	28.8
75	15	11-30	5-45	23.0
100	20	11-30	5-45	17.3
120	20	9-34	4-47	14.3
150	20	7-39	3-49	11.5
190	25	7-32	3-46	9.15
200	25	7-10	3-35	8.6
225	25	6-25	3-12	7.7
240	25	5-58	2-59	7.2
250	25	5-44	2-52	6.9
275	25	5-12	2-36	6.2
288	50	9-58	4-59	6.0
300	50	9-32	4-46	5.7
350	50	8-12	4-06	4.9
376	50	7-40	3-50	4.6
400	50	7-10	3-35	4.3
410	50	7-00	3-30	4.2

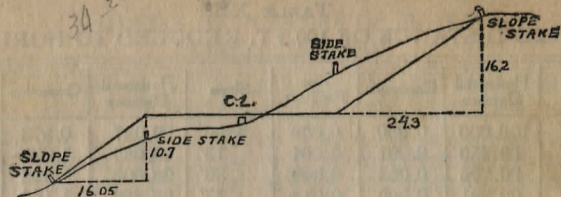
To find length of curve divide angle from P. C. to P. T. by central angle of chord, and multiply by length of chord.

TABLE XII.  
INCLINED DISTANCE OF 100 FT. REDUCED TO HORIZONTAL

Slope	Horizontal Distance	Correction	Rise Per Foot	Slope	Horizontal Distance	Correction	Rise Per Foot
0°00'	100.000	0.000	0.000	8°00'	99.027	0.973	0.139
15'	99.999	0.001	0.004	15'	98.965	1.035	0.143
30'	99.996	0.004	0.009	30'	98.902	1.098	0.148
45'	99.991	0.009	0.013	45'	98.836	1.164	0.152
1 00	99.985	0.015	0.017	9 00	98.769	1.231	0.156
15	99.976	0.024	0.022	15	98.700	1.300	0.161
30	99.966	0.034	0.026	30	98.629	1.371	0.165
45	99.953	0.047	0.031	45	98.556	1.444	0.169
2 00	99.939	0.061	0.035	10 00	98.481	1.519	0.174
15	99.923	0.077	0.039	15	98.404	1.596	0.178
30	99.905	0.095	0.044	30	98.325	1.675	0.182
45	99.885	0.115	0.048	45	98.245	1.755	0.187
3 00	99.863	0.137	0.052	11 00	98.163	1.837	0.191
15	99.839	0.161	0.057	15	98.079	1.921	0.195
30	99.813	0.187	0.061	30	97.992	2.008	0.199
45	99.786	0.214	0.065	45	97.905	2.095	0.204
4 00	99.756	0.244	0.070	12 00	97.815	2.185	0.208
15	99.725	0.275	0.074	15	97.723	2.277	0.212
30	99.692	0.308	0.078	30	97.630	2.370	0.216
45	99.657	0.343	0.083	45	97.534	2.466	0.221
5 00	99.619	0.381	0.087	13 00	97.437	2.563	0.225
15	99.580	0.420	0.092	15	97.338	2.662	0.229
30	99.540	0.460	0.096	30	97.237	2.763	0.233
45	99.497	0.503	0.100	45	97.134	2.866	0.238
6 00	99.452	0.548	0.105	14 00	97.030	2.970	0.242
15	99.406	0.594	0.109	15	96.923	3.077	0.246
30	99.357	0.643	0.113	30	96.815	3.185	0.250
45	99.307	0.693	0.118	45	96.705	3.295	0.255
7 00	99.255	0.745	0.122	15 00	96.593	3.407	0.259
15	99.200	0.800	0.126	15	96.479	3.521	0.263
30	99.144	0.856	0.131	30	96.363	3.637	0.267
45	99.087	0.913	0.135	45	96.246	3.754	0.271

TABLE XIII.  
MINUTES IN DECIMALS OF A DEGREE.

0 30"	.00833	10' 30"	.17500	20' 30"	.34167	30' 10"	.50833	40' 30"	.67500	50' 10"	.84167
1 00	.01667	11 00	.18333	21 00	.35000	31 00	.51667	41 00	.68333	51 00	.85000
30	.02500	30	.19167	30	.35833	30	.52500	30	.69167	30	.85833
2 00	.03333	12 00	.20000	22 00	.36667	32 00	.53333	42 00	.70000	52 00	.86667
30	.04167	30	.20833	30	.37500	30	.54167	30	.70833	30	.87500
3 00	.05000	13 00	.21667	23 00	.38333	33 00	.55000	43 00	.71667	53 00	.88333
30	.05833	30	.22500	30	.39167	30	.55833	30	.72500	30	.89167
4 00	.06667	14 00	.23333	24 00	.40000	34 00	.56667	44 00	.73333	54 00	.90000
30	.07500	30	.24167	30	.40833	30	.57500	30	.74167	30	.90833
5 00	.08333	15 00	.25000	25 00	.41667	35 00	.58333	45 00	.75000	55 00	.91667
30	.09167	30	.25833	30	.42500	30	.59167	30	.75833	30	.92500
6 00	.10000	16 00	.26667	26 00	.43333	36 00	.60000	46 00	.76667	56 00	.93333
30	.10833	30	.27500	30	.44167	30	.60833	30	.77500	30	.94167
7 00	.11667	17 00	.28333	27 00	.45000	37 00	.61667	47 00	.78333	57 00	.95000
30	.12500	30	.29167	30	.45833	30	.62500	30	.79167	30	.95833
8 00	.13333	18 00	.30000	28 00	.46667	38 00	.63333	48 00	.80000	58 00	.96667
30	.14167	30	.30833	30	.47500	30	.64167	30	.80833	30	.97500
9 00	.15000	19 00	.31667	29 00	.48333	39 00	.65000	49 00	.81667	59 00	.98333
30	.15833	30	.32500	30	.49167	30	.65833	30	.82500	30	.99167
10 00	.16667	20 00	.33333	30 00	.50000	40 00	.66667	50 00	.83333	60 00	1.00000



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0 30	0 45	0 60	0 75	0 90	1 05	1 20	1 35	0
1	1 50	1 65	1 80	1 95	2 10	2 25	2 40	2 55	2 70	2 85	1
2	3 00	3 15	3 30	3 45	3 60	3 75	3 90	4 05	4 20	4 35	2
3	4 50	4 65	4 80	4 95	5 10	5 25	5 40	5 55	5 70	5 85	3
4	6 00	6 15	6 30	6 45	6 60	6 75	6 90	7 05	7 20	7 35	4
5	7 50	7 65	7 80	7 95	8 10	8 25	8 40	8 55	8 70	8 85	5
6	9 00	9 15	9 30	9 45	9 60	9 75	9 90	10 05	10 20	10 35	6
7	10 50	10 65	10 80	10 95	11 10	11 25	11 40	11 55	11 70	11 85	7
8	12 00	12 15	12 30	12 45	12 60	12 75	12 90	13 05	13 20	13 35	8
9	13 50	13 65	13 80	13 95	14 10	14 25	14 40	14 55	14 70	14 85	9
10	15 00	15 15	15 30	15 45	15 60	15 75	15 90	16 05	16 20	16 35	10
11	16 50	16 65	16 80	16 95	17 10	17 25	17 40	17 55	17 70	17 85	11
12	18 00	18 15	18 30	18 45	18 60	18 75	18 90	19 05	19 20	19 35	12
13	19 50	19 65	19 80	19 95	20 10	20 25	20 40	20 55	20 70	20 85	13
14	21 00	21 15	21 30	21 45	21 60	21 75	21 90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23 10	23 25	23 40	23 55	23 70	23 85	15
16	24 00	24 15	24 30	24 45	24 60	24 75	24 90	25 05	25 20	25 35	16
17	25 50	25 65	25 80	25 95	26 10	26 25	26 40	26 55	26 70	26 85	17
18	27 00	27 15	27 30	27 45	27 60	27 75	27 90	28 05	28 20	28 35	18
19	28 50	28 65	28 80	28 95	29 10	29 25	29 40	29 55	29 70	29 85	19
20	30 00	30 15	30 30	30 45	30 60	30 75	30 90	31 05	31 20	31 35	20
21	31 50	31 65	31 80	31 95	32 10	32 25	32 40	32 55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33 60	33 75	33 90	34 05	34 20	34 35	22
23	34 50	34 65	34 80	34 95	35 10	35 25	35 40	35 55	35 70	35 85	23
24	36 00	36 15	36 30	36 45	36 60	36 75	36 90	37 05	37 20	37 35	24
25	37 50	37 65	37 80	37 95	38 10	38 25	38 40	38 55	38 70	38 85	25
26	39 00	39 15	39 30	39 45	39 60	39 75	39 90	40 05	40 20	40 35	26
27	40 50	40 65	40 80	40 95	41 10	41 25	41 40	41 55	41 70	41 85	27
28	42 00	42 15	42 30	42 45	42 60	42 75	42 90	43 05	43 20	43 35	28
29	43 50	43 65	43 80	43 95	44 10	44 25	44 40	44 55	44 70	44 85	29
30	45 00	45 15	45 30	45 45	45 60	45 75	45 90	46 05	46 20	46 35	30
31	46 50	46 65	46 80	46 95	47 10	47 25	47 40	47 55	47 70	47 85	31
32	48 00	48 15	48 30	48 45	48 60	48 75	48 90	49 05	49 20	49 35	32
33	49 50	49 65	49 80	49 95	50 10	50 25	50 40	50 55	50 70	50 85	33
34	51 00	51 15	51 30	51 45	51 60	51 75	51 90	52 05	52 20	52 35	34
35	52 50	52 65	52 80	52 95	53 10	53 25	53 40	53 55	53 70	53 85	35
36	54 00	54 15	54 30	54 45	54 60	54 75	54 90	55 05	55 20	55 35	36
37	55 50	55 65	55 80	55 95	56 10	56 25	56 40	56 55	56 70	56 85	37
38	57 00	57 15	57 30	57 45	57 60	57 75	57 90	58 05	58 20	58 35	38
39	58 50	58 65	58 80	58 95	59 10	59 25	59 40	59 55	59 70	59 85	39
40	60 00	60 15	60 30	60 45	60 60	60 75	60 90	61 05	61 20	61 35	40
41	61 50	61 65	61 80	61 95	62 10	62 25	62 40	62 55	62 70	62 85	41
42	63 00	63 15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64 35	42
43	64 50	64 65	64 80	64 95	65 10	65 25	65 40	65 55	65 70	65 85	43
44	66 00	66 15	66 30	66 45	66 60	66 75	66 90	67 05	67 20	67 35	44
45	67 50	67 65	67 80	67 95	68 10	68 25	68 40	68 55	68 70	68 85	45
46	69 00	69 15	69 30	69 45	69 60	69 75	69 90	70 05	70 20	70 35	46
47	70 50	70 65	70 80	70 95	71 10	71 25	71 40	71 55	71 70	71 85	47
48	72 00	72 15	72 30	72 45	72 60	72 75	72 90	73 05	73 20	73 35	48
49	73 50	73 65	73 80	73 95	74 10	74 25	74 40	74 55	74 70	74 85	49
50	75 00	75 15	75 30	75 45	75 60	75 75	75 90	76 05	76 20	76 35	50

Computed by L. Leland Locke.

74.4  
 23 28  
 20 94 → 11.6  
 228 55 34  
 36  
 203.37  
 189.45  
 13.89  
 39.52  
 1385.70  
 1425.22  
 74.78  
 11.7  
 5.4  
 6.3  
 79.88  
 60.  
 139.88  
 70  
 37  
 33  
 67  
 950.5  
 869  
 3.381.5  
 1.4  
 1.9  
 19.90  
 11.5  
 3.4  
 8.1  
 21  
 49  
 20  
 15  
 282.10  
 5257.88  
 5539.98  
 131.6  
 1040 Shuck Rd  
 North  
 679  
 I.P.

38.40  
 36.46  
 5 up

PLEASE RETURN TO  
 GAUGA COUNTY ENGINEER  
 COURT HOUSE  
 CHARDON, O.  
 PHONE 250 X

TABLE OF INCHES REDUCED TO DECIMALS OF A FOOT.

Ins.	Dec.	Ins.	Dec.	Ins.	Dec.	Ins.	Dec.	Ins.	Dec.	Ins.	Dec.	Ins.	Dec.
1	.0000	11	.8800	21	.1680	31	.2520	41	.3360	51	.4200	61	.5040
2	.0020	12	.8960	22	.1760	32	.2640	42	.3480	52	.4320	62	.5160
3	.0040	13	.9120	23	.1840	33	.2720	43	.3560	53	.4400	63	.5240
4	.0060	14	.9280	24	.1920	34	.2800	44	.3640	54	.4480	64	.5320
5	.0080	15	.9440	25	.2000	35	.2880	45	.3720	55	.4560	65	.5400
6	.0100	16	.9600	26	.2080	36	.2960	46	.3800	56	.4640	66	.5480
7	.0120	17	.9760	27	.2160	37	.3040	47	.3880	57	.4720	67	.5560
8	.0140	18	.9920	28	.2240	38	.3120	48	.3960	58	.4800	68	.5640
9	.0160	19	.1000	29	.2320	39	.3200	49	.4040	59	.4880	69	.5720
10	.0180	20	.1080	30	.2400	40	.3280	50	.4120	60	.4960	70	.5800
11	.0200	21	.1160	31	.2480	41	.3360	51	.4200	61	.5040	71	.5880
12	.0220	22	.1240	32	.2560	42	.3440	52	.4280	62	.5120	72	.5960
13	.0240	23	.1320	33	.2640	43	.3520	53	.4360	63	.5200	73	.6040
14	.0260	24	.1400	34	.2720	44	.3600	54	.4440	64	.5280	74	.6120
15	.0280	25	.1480	35	.2800	45	.3680	55	.4520	65	.5360	75	.6200
16	.0300	26	.1560	36	.2880	46	.3760	56	.4600	66	.5440	76	.6280
17	.0320	27	.1640	37	.2960	47	.3840	57	.4680	67	.5520	77	.6360
18	.0340	28	.1720	38	.3040	48	.3920	58	.4760	68	.5600	78	.6440
19	.0360	29	.1800	39	.3120	49	.4000	59	.4840	69	.5680	79	.6520
20	.0380	30	.1880	40	.3200	50	.4080	60	.4920	70	.5760	80	.6600
21	.0400	31	.1960	41	.3280	51	.4160	61	.5000	71	.5840	81	.6680
22	.0420	32	.2040	42	.3360	52	.4240	62	.5080	72	.5920	82	.6760
23	.0440	33	.2120	43	.3440	53	.4320	63	.5160	73	.6000	83	.6840
24	.0460	34	.2200	44	.3520	54	.4400	64	.5240	74	.6080	84	.6920
25	.0480	35	.2280	45	.3600	55	.4480	65	.5320	75	.6160	85	.7000
26	.0500	36	.2360	46	.3680	56	.4560	66	.5400	76	.6240	86	.7080
27	.0520	37	.2440	47	.3760	57	.4640	67	.5480	77	.6320	87	.7160
28	.0540	38	.2520	48	.3840	58	.4720	68	.5560	78	.6400	88	.7240
29	.0560	39	.2600	49	.3920	59	.4800	69	.5640	79	.6480	89	.7320
30	.0580	40	.2680	50	.4000	60	.4880	70	.5720	80	.6560	90	.7400
31	.0600	41	.2760	51	.4080	61	.4960	71	.5800	81	.6640	91	.7480
32	.0620	42	.2840	52	.4160	62	.5040	72	.5880	82	.6720	92	.7560
33	.0640	43	.2920	53	.4240	63	.5120	73	.5960	83	.6800	93	.7640
34	.0660	44	.3000	54	.4320	64	.5200	74	.6040	84	.6880	94	.7720
35	.0680	45	.3080	55	.4400	65	.5280	75	.6120	85	.6960	95	.7800
36	.0700	46	.3160	56	.4480	66	.5360	76	.6200	86	.7040	96	.7880
37	.0720	47	.3240	57	.4560	67	.5440	77	.6280	87	.7120	97	.7960
38	.0740	48	.3320	58	.4640	68	.5520	78	.6360	88	.7200	98	.8040
39	.0760	49	.3400	59	.4720	69	.5600	79	.6440	89	.7280	99	.8120
40	.0780	50	.3480	60	.4800	70	.5680	80	.6520	90	.7360		
41	.0800	51	.3560	61	.4880	71	.5760	81	.6600				
42	.0820	52	.3640	62	.4960	72	.5840	82	.6680				
43	.0840	53	.3720	63	.5040	73	.5920	83	.6760				
44	.0860	54	.3800	64	.5120	74	.6000	84	.6840				
45	.0880	55	.3880	65	.5200	75	.6080	85	.6920				
46	.0900	56	.3960	66	.5280	76	.6160	86	.7000				
47	.0920	57	.4040	67	.5360	77	.6240	87	.7080				
48	.0940	58	.4120	68	.5440	78	.6320	88	.7160				
49	.0960	59	.4200	69	.5520	79	.6400	89	.7240				
50	.0980	60	.4280	70	.5600	80	.6480	90	.7320				
51	.1000	61	.4360	71	.5680	81	.6560	91	.7400				
52	.1020	62	.4440	72	.5760	82	.6640	92	.7480				
53	.1040	63	.4520	73	.5840	83	.6720	93	.7560				
54	.1060	64	.4600	74	.5920	84	.6800	94	.7640				
55	.1080	65	.4680	75	.6000	85	.6880	95	.7720				
56	.1100	66	.4760	76	.6080	86	.6960	96	.7800				
57	.1120	67	.4840	77	.6160	87	.7040	97	.7880				
58	.1140	68	.4920	78	.6240	88	.7120	98	.7960				
59	.1160	69	.5000	79	.6320	89	.7200	99	.8040				
60	.1180	70	.5080	80	.6400	90	.7280						
61	.1200	71	.5160	81	.6480								
62	.1220	72	.5240	82	.6560								
63	.1240	73	.5320	83	.6640								
64	.1260	74	.5400	84	.6720								
65	.1280	75	.5480	85	.6800								
66	.1300	76	.5560	86	.6880								
67	.1320	77	.5640	87	.6960								
68	.1340	78	.5720	88	.7040								
69	.1360	79	.5800	89	.7120								
70	.1380	80	.5880	90	.7200								
71	.1400	81	.5960	91	.7280								
72	.1420	82	.6040										
73	.1440	83	.6120										
74	.1460	84	.6200										
75	.1480	85	.6280										
76	.1500	86	.6360										
77	.1520	87	.6440										
78	.1540	88	.6520										
79	.1560	89	.6600										
80	.1580	90	.6680										
81	.1600	91	.6760										
82	.1620	92	.6840										
83	.1640	93	.6920										
84	.1660	94	.7000										
85	.1680	95	.7080										
86	.1700	96	.7160										
87	.1720	97	.7240										
88	.1740	98	.7320										
89	.1760	99	.7400										
90	.1780												
91	.1800												
92	.1820												
93	.1840												
94	.1860												
95	.1880												
96	.1900												
97	.1920												
98	.1940												
99	.1960												
100	.1980												

B. K. ELLIOTT COMPANY, PITTSBURG, PA.  
 DRAWING MATERIALS AND SURVEYING INSTRUMENTS

